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The demand of the world's economy for energy I S ever increasing. Wells in the same field can be classified as gas wells, condensate wells, and oil wells. 1.2 Utilization of Natural Gas the spreadsheet Carr-KobayashiBurrows Viscosity.xls that is attached to this book. The net result is that the flow rates calculated for the 100 percent efficiency factor E. This chapter focuses on determination of gas properties with correlations developed from various lab measurements. With the trend to higher operating pressures in transmission lines, the need for these factors is greater than is generally realized. Future gas supplies as a ratio of the amount of oil to be discovered is a method that has been used also. 0.02 38 Chapter 3 Gas Reservoir Deliverability &OLFNWR9LHZ&DOFXODWLRQ([DPSOH Table 3-2 Results Given by Theoretical Deliverability.xls Solution 1) Based on the property table, enter a value for the real gas pseudopressure at pressure 3,000 psia 604,608,770 psi2/cp; 2) Run Macro Solution to get result. The rapidly growing energy demands of Western Europe, Japan, and the United States could not be satisfied without importing gas t r o ~ nfar fields. Gonzalez, and B. Natural gas is one of the major fossil energy sources. It will likely cause chronic energy shortage as early as 201 0. "Density of Natural Gases." Trans. 1.8 Problems 1-2 Natural gas from the William County, North Dakota, Red River formation, has a heating value of 1,032 Btulscf. The shale is generally fissile, finely laminated, and varicolored but predominantly black, brown, or greenish-gray. For the convenience of engineering applications, the normalized gas pressures and temperatures have been generated with the spreadsheet program NormP.xls. A thorough assessment of the internal corrosion mechanism and rate is necessary before any corrosion allowance is taken. The well was tested at two flow rates: 1 Test point 1 I 1,548 MscWd I Bottom hole pressure: 697 psia Pseudocritical pseudocri temperature: 345 O R Pseudo-reduced pressure: 7.17 Pseudo-reduced temperature: 1.85 Gas compressibility factor z: 0.9780 This spreadsheet calculates gas compressibility factor based on Brill and Beggs correlat~on. 11 Chapter 2 Properties of Natural Gas 2.1 Introduction Properties of natural gas include gas-specific gravity, pseudocritical pressure and temperature, viscosity, compressibility factor, gas density, and gas compressibility. Beggs. Natural gas is the fuel that is superior to other energy sources not only in economic attractiveness but also in environmental concerns. They showed that, while neglecting the special gas storage and flow properties in the short term is appropriate such neglect in the long term will result in an underestimation of gas production. Appendix C presents orifice meter tables for natural gases. P., and H. Although the principles of natural gas production. Appendix C presents of the principles of natural gas production. Appendix C presents of the principles of natural gas production. Appendix C presents of the principles of the pri play a crucial role in engineering design and analyses. Gas desorbs from the surface of the kerogenlclays. paper) 1. H. Eakin. 2.5 Compressibility factor is also called deviation factor, or z-factor. Data from three typical wells plotted in 56 Chapter 3 Gas Reservoir Deliverability Figure 3-5. Applying the Weymouth equation to each of the three segments gives: Adding equations (11.43), (1 1.44), and (1 1.45) gives: Capacity of a single-diameter (DI) pipeline is expressed as: Dividing Equation (1 1.47) by Equation (1 1.47) by Equation (1 1.47) by Equation (1 1.47) by Equation (1 1.49) yields: Figure 11-2 Sketch of series pipeline. 2.8 Compressibility of Natural Gas Gas compressibility is defined as: nzRT Because the gas law for real gas gives V = -, P Substituting Equation (2.50) into Equation (2.49) yields: 28 Chapter 2 Properties of Natural Gas 2.9 Real Gas Pseudopressure m(p) is defined as where pb is the base pressure (14.7 psia in most states in the U.S.). 2.2 Specific Gravity Gas-specific gravity (&) is defined as the ratio of the apparent molecular Shale Gas Wells 3.8 Well Deliverability Testing 56 3.8.1 Flow-After-Flow Test 57 3.8.2 Isochronal Test 59 3.8.3 Modified Isochronal Test 61 50 54 4 Wellbore Performance67 4.1 Introduction 4.2 Single-Phase Gas Well 68 Factor 4.2.1 The Average Temperature and Compress~bil~ty Method 68 4.2.2 The Cullender 3.6 Multi-Fractured Horizontal Wells 5 1 2 Reservoir linear flow between fractures in the reservoir to the fracture faces. They can be proved by known reservoir characteristics such as production data, pressure relationships, and other and Smith Method 72 67 4.3 Mist Flow in Gas Wells 74 5 Choke Performance data, so that volumes of gas can be determined with reasonable accuracy. Example Problem 3.1 A gas well produces 0.65 specific gravity natural gas with N P, C02, and H2S of mole fractions 0.1, 0.08, and 0.02, respectively. Some gases are called gas condensates or simply condensates. 2.10 Real Gas Normalized Pressure 31 &OLFNWR9LHZ&DOFXODWLRQ([DPSOH Table 2-6 Partial Output Given by PseudoP.xls 32 Chapter 2 Properties of Natural Gas 2.1 1 References Ahmed, T. Equation (11.62) can be rearranged to solve for X explicitly: 11.2 Pipeline Design 247 The effects of looped line on the increase of gas flow rate for various pipe diameter ratios are shown in Figure 11-4. Updated and enhanced from the best-selling First Edition, this book continues to provide upcoming and practicing engineers the full scope of natural gas engineering, from gas reservoirs to transportation with a computer-assisted approach. Dehydration 9. The average pressure is: p = (200 + 600)12 = 400 psia With p = 400 psia, T = 540 OR, and yg = 0.70, Brill-Beggs-Z.xls gives: With p = 400 psia, T = 540 OR, and yg = 0.70, Carr-KobayashiBurrows Viscosity.xls gives: Relative roughness: e~ = 0.0006112.09 = 0.00005 11.2 A. Hence, with When a pipeline is designed using the collapse criterion, a good knowl. Solution This problem is solved with the spreadsheet program Theoretical Deliverability.xls. Accurate modeling of long-term well performance requires application of unconventional properties to simulate the semi-infinite flow behavior. Gas well IPR also depends on flow conditions, that is, transient, steady state, or pseudosteady state flow, which are determined by reservoir boundary conditions. The way to avoid such a crunch is to expand energy supply and move from oil to natural gas and, eventually, to hydrogen. As demonstrated by Guo and Y u (2008), predictions of the long-term productivity of multi-fractured horizontal wells must consider the following sequence: 1 Reservoir radial flow within the drainage boundary to the fractured region of reservoir. Input Data Effective permeability to gas: 0.17 md Pay zone thickness: 78 ft Equivalent drainage radius: 1,490 ft Wellbore radius: 0.328 ft Darcy skin factor: 5 Non-Darcy coefficient: 0.001 d/Mscf Reservoir pressure: 4,613 psia Flowing bottom hole pressure: 3,000 psia Temperature: 180 OF Gas-spec~ficgravity: 0.65 1 for air .- Mole fract~onof N2: 0.1 Mole fraction of C02: Mole fraction of H2S: a. Hydrocarbon Phase Behavior. Figure 1-1 shows that during the three-year period 2000-02, natural gas consumption was equitably distributed across all sectors of the U.S. economy (cxxcepttransportation). 2. McCain, W. 2.7 Formation Volume Factor and Expansion Factor Formation volume factor is defined as the ratio of gas volume at reservoir condition to the gas volume at standard condition, that is, where the unit of formation volume factor is ft3/scf. 11.2.2.1 Design Procedure Determination of pipeline wall thickness is based on the design-internal pressure or the external hydrostatic pressure. It drains gas from a 78-ft thick pay zone in an area of 160 acres. Except for large diameter pipes (over 30 in), material grade is usually taken as X-60 or X-65 (414 or 448 MPa) for high-pressure pipelines. Figure 3-7 shows the data plot and technique for deriving the C' and n values from the flow-after-flow test. In Equation (1 1.64), the weld efficiency factor (E,) is 1.0 for seamless, ERW, and DSAW pipes. 3.6 Multi-Fractured Horizontal Wells Some low-productivity horizontal wells, such as those in shale gas reservoirs, are purposely drilled in parallel to the direction of the minimum horizontal stress in the formation. Choke Performance 6. There are three types of natural gases: nonassociated gas, associated gas, and gas condensate. Flow rates and pressures follow the pattern depicted in Figure 3-6. HOUSTON, TX: Gulf Publishing Company 2 Greenway Plaza, Suite 1020 Houston, TX 77046 ISBN- 13: 978- 1-933-762-21-8 I 0 9 8 7 6 5 4 3 2 Library of Congress Cataloging-in-PublicationData Cuo, Boyun. This non-equilibrium process further drives the gas molecules to diffuse from the bulk of the kerogen to the surface of the kerogen exposed to the pore network. There has been a huge disparity between "proven" rcserves and potential reserved. This book is written primarily for natural gases. All rights reserved. This book is written primarily for natural gases. All rights reserved. This book is written primarily for natural gases. All rights reserved. This book is written primarily for natural gases. Methods Very often it is difficult and costly to obtain values of all the parameters in equations (3.1), (3.3), and (3.4). The well is then flowed at a second rate for the same length of time, followed by another shut-in, The process is repeated for a total of 3 to 4 rates. of natural gas. Gases in tight shales are found in the eastern United States (Kentucky, Ohio, Virginia, and West Virginia). 78 ft This spreadsheet calculates and plots theoretical gas well IPR curves. Figure 1-4 U.S. natural gas price from 1978 to 2010 (Louisiana Department of Natural Resources 2011). Otherwise. Figure 3-10 illustrates the technique for obtaining the C and n values from the isochronal test. Equation (3.1) can then be simplified using a pressure-squared approach such as: At pressures higher than 3,000 psia, highly compressed gases behave like liquids. "Calculate Zs for Sour Gases." Hydrocarbon Processing 51 (May 1972): 119. Other so-called alternative energy sources have little chance to compete with natural gas. 1.4 Natural Gas Reserves Two terms are frequently used to express natural gas reserves: proved reserves and potential resources. A value of 1/16 inch may be appropriate. The recent engineering achievements in multi-stage fractures in long horizontal well laterals have inevitably increased the interest in exploitation of shale gas reservoirs. 7 0 9x - 2.062 K 10 - v_y , (2.19) 2.4 Dempsey (1965) developed the following relation: where (LO = -2.4621 1820 tx, = 2.970547 14 (12 = -0.28626405 tr3 = 0.00805420 (14 = 2.80860949 (15 = -3.49803305 = 0.36037302 1 ~ 7 = -0.01044324 (18 = -0.79338568 ag = 1.39643306 crlo = -0.14914493 rr, = -0. 0.00441016 rr 1, = 0.08393872 (1 13 = -0.18640885 (1 14 = 0.02033679 1, = -0.00060958 Viscosity 19 20 Chapter 2 Properties of Natural Gas Thus, once the value of pr is determined from the right-hand side of this equation, gas viscosity at elevated pressure can be readily calculated using the following relation: Other correlations for gas viscosity include Dean-Stiel (1958) and LeeGonzalez-Eakin (1966). These two parameters, plus the nonDarcy flow coefficient D, can be used to simulate choked fracture. Nonassociated gas is found in a reservoir that contains a minimal quantity of crude oil. Account should be taken of substantial pipeline elevation changes. The rate is then changed and the well flows until the pressure stabilizes again at the new rate. T it le. When a pipeline is designed based on the collapse criteria, buckle arrestors are recommended. This spreadsheet computes capacities of series, parallel, and looped pipelines (see Example Problem 11.2). If this gas is combusted to drive a gas turbine for a gas compressor of 1,000 hp,361 Contents ix E The Minimum Gas Production Rate for Condensate Removal in Gas Wells what is the required gas flow rate in MMscfIday? DOEIEIA. 325 D The Minimum Gas Production Rate for Water Removal in Gas Wells413 F Mathematical Model for Obtaining Correction Factor Fg ...465 Chapter I Introduction 1.1 What Is Natural Gas? 1,I 88,000 cfh 3,335,270 0.01143 0 1,076,035 cfh This program computes the capacity of gas pipelines (see Example Problem 11. The value of n is usually between 0.5 and 1 . Joshi's equation was modified by Economides et al. Gas is stored as compressed gas in pores, as adsorbed gas to the pore walls and as soluble gas in solid organic materials and clays. 2.3 Pseudocritical Pro~erties 15 Example Problem 2.1 For the gas composition given in the following text, determine apparent molecular weight, pseudocritical pressure, and pseudocritical temperature of the gas. This means that the natural gas share of the energy mix will increase from 23 percent to over 28 percent. New York: John Wiley & Sons, 1984. Example Problem 2.2 A 0.65 specific gravity natural gas contains 10% nitrogen, 8% carbon dioxide, and 2% hydrogen sulfide. Both analytical methods are discussed. Gas condensate refers to gas with high content of liquid hydrocarbon at reduced pressures and temperatures. A Ramberg Osgood relationship can be used: where $K^* = K/K$, and $M^* = M/My$ with Ky = 2Sy/ED is the yield curvature and My = 21Sy/D is the yield curvature and My = 21Sy/D is the yield curvature and My = 21Sy/D is the yield moment. In length, the band extends from Florida to Texas; in width, it extends from Florida to Texas; in width, it extends from Florida to Texas; in width, it extends from A moment. Corrosion Allowance Extra wall thickness is added to account for corrosion when water is present in a fluid along with contaminants such as oxygen, hydrogen sulfide (H2S), and carbon dioxide (C02). Burrows. For a given amount of gas, if temperature is kept constant and volume is measured at 14.7 psia and an elevated pressure pl, z-factor can then be determined with the following formula: where Vo and V, are gas volumes measured at 14.7 psia and pl, respectively. The mission of the book is to provide engineers a hand) guideline to designing, analyzing, and optimizing natural gas production and processing systems. The phenomena of gas storage and flow in shale gas sediments are believed to be a combination of different controlling processes. In the United States they are located predominantly both onshore and offshore in a band along the Gulf of Mexico (Ikoku 1984). Kobayashi, and D. Printed in the United States of America Printed on acid-free paper. This can be done for large orders. The average reservoir pressure 3.2 Analytical Methods 37 is 4,613 psia. Calculated gas viscosities, z-factors, and pseudopressures at pressures between 9,950 psia and 10,000 psia are presented in Table 2-6. Commercial 13.76% Industrial 38.16% Residential 21.58% Utility 23.65% Figure 1-1 Natural gas is used as a source of energy in all sectors of the U.S. economy (Louisiana Department of Natural Resources 2004). D = 12.09 in L = 200 mi e = 0.0006 nT = 80 OF rg = 0.70 Tb = 520 OR pb = 14.7 psia pl = 600 psia p2 = 200 psia Solution The problem can be solved using Equation (11.22) with the trialand-error method for friction factor and the Weymouth equation without the Reynolds number-dependent friction factor. The appearance of the first section of the spreadsheet is shown in Table 3-1. It is thought, therefore, that the majority of production is controlled by bedding planes and jointing (Ikoku 1984). The atmospheric value is then adjusted to pressure conditions by means of a correction factor on the basis of reduced temperature and pressure state of the gas. Conventional natural gas is either associated or nonassociated gas. Estimate viscosity of the gas at 10,000 psia and 180 OF. 2001). L., M. Pure methane would have a gravity equal to (16.04128.97) = 0.55. The under-thickness due to manufacturing tolerance is taken into account in the design factor. Katz. It assumes that f varies as: and it takes the following resultant form: 11.2.1.5.5 Clinedinst Equation-Horizontal Flow The Clinedinst Equation rigorously considers the deviation of natural gas from ideal gas through integration. The U.S. demand for natural gas from ideal gas through integration rigorously considers the deviation of natural gas from ideal gas through integration. 14). I. The twentieth century was the century of oil that was the primary energy source to support the growth of global economy. L. and K. "Two-Phase Flow in Pipes." INTERCOMP Course, The Hague, 1974. Including prefabricated or retrofit sections and pipeline section in a J-tube. There is no need to add any allowance for fabrication to the wall thickness calculated with Equation (1 1.64). This book was intended to cover the full scope of natural gas production engineering. The appearance of the first section of the spreadsheet is shown in Table 3-3. Example problems are presented and solved using computer programs provided with this book. New York: Marcel Dekker Inc., 1990. At higher gas permeabilities, the formations are generally amenable to conventional fracturing and completion methods. The aspect ratio (length to width) of the drainage area may be taken as and the shape factor may be estimated as CA = 39.51-8.5214RA. Figure 1-3 presents U.S. natural gas production history. Gas hydrates, discovered in 1810, are snow-like solids in which each water molecule forms hydrogen bonds with the four nearest water molecules to build a crystalline lattice structure that traps gas molecules in its cavities (Sloan 1990). 44 Chapter 3 Gas Reservoir Deliverability & OLFNWR9LHZ&DOFXODWLRQ([DPSOH Table 3-5 -- Input Data Given by Theoretical IPR.xlsa -- Instructions: 1) Update input data; 2) Run Macro Solution and view result and plot. "The Viscosity of Non-polar Gas Mixtures at Moderate and High Pressures." AIChE Journal 4 (1958): 430-6. If this gas is combusted to generate power of 1,000 kW, what is the required gas flow rate in Mscflday? bottom hole pressure: 1,685 psia Flowing bottom hole pressure: 1,050 psia Temperature: 180 "F Gas-specif~cgravity: 0.65 1 for air Mole fraction of N2: 0.1 Mole fraction of C02: 0.08 Mole fraction of H2S: 0.02 This spreadsheet calculates gas reservoir deliverability with empirical models. Because natural gas is petroleum in a gaseous state, it is always accompanied by oil that is liquid petroleum. Figure 11-4 Effects of looped line and pipe diameter ratio on the increase of gas flow rate. As regards prc, sentation, this book focuses on presenting principles, criteria, basic data, and spreadsheet programs necessary to quickly perform engineerin: a~alyses. &OLFNWR9LHZ&DOFXODWLRQ([DPSOH Table 2 4 Results Given by Hall-Yarborogh-z.xlsa Instructions: 1) Input data; 2) Run Macro Solution; 3) View result. (1996) presented an analytical model for predicting productivities of horizontal wells with multiple transverse fractures. 3.3 Empirical Methods 41 &OLFNWR9LHZ&DOFXODWLRQ([DPSOH Table 3-3 The First Section of Empirical Deliverability.xlsa Instructions: 1) Go to the Solution section and enter values for real gas pseudopressureat the tested and desired flowing bottom hole pressures; 2) Run Macro Solution, and view results. This chart has been set up for computer solution by a number of individuals. The result is shown in Table 2-3. R. Separation 8. Chapter 2 document\ pioperties of natural gases that are essential for designing and analyzing natural gas production and processing systems. Compare the results with that given by the Brill and Beggs' correlation. Gas production from a newly drilled wellbore is through the large pores and then the smaller pores. 3.2 Analytical Methods A general solution to pseudosteady state flow in a radial-flow gas reservoir is expressed as (Economides 1994): where q is the gas production rate in Mscftd, k is the effective permeability to gas in md, h is the thickness of pay zone in ft, m(p) is the real gas pseudopressure in psi2/cp at the reservoir pressure p in psi, m(pwf) is the real gas pseudopressure in psi2/cp at the flowing bottom hole pressure 36 Chapter 3 Gas Reservoir Deliverability p,f, T is the reservoir temperature in R, yw is the radius of drainage area in ft, yw is wellbore radius in ft, s is skin factor, and D is the non-Darcy coefficient in dlMscf. If you are author/publisher or own the copyright of this documents, please report to us by using this DMCA report form. 11.2.2.2.2.1 Propagation Criteria Although a large number of empirical relationships have been published, the recommended formula is the latest given by AGA (1990): The nominal wall thickness should be determined such that: The safety factor of 1.3 is recommended to account for uncertainty in the envelope of data points used to derive Equation (1 1.65). Natural gas engineering handbook / Boyun Cuo, A l i Ghalambor. 1.6 Future of the Natural Gas Industry It is well recognized that the nineteenth century of coal that supported the initiation of industrial revolution in Europe. Table 11-3 Transmission Factors for Pipeline Flow Equations Flow Equations Flow Equations Flow Equation of industrial revolution in Europe. Panhandle A Panhandle B 11.2.1.6.3 Empirical Pipeline Equation A general noniterative pipeline flow equation is written as 11.2 Pipeline Design 241 where the units are q in cfd measured at Tb and p,, T in OR, p in psia, L in miles, and D in inches. Petroleum engineering-Handbooks, manuals, etc. 11.3 Transportation of LNG 257 For design purposes, condition oh E-Book Information Year: 2,012 Edition: 2nd Edition Pages: 310 Identifier: 978-0-7844-7110-4,978-0-7844-0731-8,1-933762-41-1 Commentary: 5,188 Org File Size: 13,635,600 Extension: pdf 256 Chapter 11 Transportation Under high bending loads, care should be taken in estimating gb using an appropriate moment-curvature relationship. 1.8 Problems 1-1 Natural gas from the Morgan County, Colorado, D-Sand, has a heating value of 1,228 Btulscf. 11.2.2.2.2.2 Collapse Criteria The mode of collapse is a function of D/t ratio, pipeline imperfections, and load conditions. Gas hydrates contain about 170 times the natural gas by volume under standard conditions. The objective of these tests is to deliver values of C and n or A and B that are used for defining well inflow performance relationship (IPR). Solution This problem is solved with the spreadsheet program Empirical IPR.xls. They take the following forms, respectively: and 3.3 Emvirical Methods 39 where A, R, C, and n are empirical constants that can be determined based on test points. E. The authors are grateful to the university for permission to publish the materials. Natural gas, liquefied by a refrigeration cycle, can now he I ransported efficiently and rapidly across the oceans of the world by insulated tankers. AIME 146: (1954) 140-9. "The Viscosity of Natural Gases." Journal of Petroleum Technology (Aug Natural gas is in this way reduced to about 1.4 Natural Gas Reserves 5 one six-hundredth of its original volume and the nonmethane components are largely eliminated. Derivation of mathematical models is beyond the scope of th ~ shook. If the pipeline is long enough, the changes in the kinetic-energy term can be neglected. On the global scale, it is more difficult to give a good estimate of natural gas reserves. 11.2 Pipeline Design for External Pressure Criteria. 11.2.2.2 Pipeline Design for External Pressure C ASME B31.8 (1989) and DnV (1981). Solution This problem is solved with the spreadsheet program Theoretical IPR.xls. - 2nd ed. I n actual pipelines, water, condensates, and sometimes crude oil accumulate i n low spots in the line. 48 Chapter 3 Gas Reservoir Deliverability & OLFNWR9LHZ&DOFXODWLRQ([DPSOH Table 3-8 Results Given by Empirical 1PR.xls q (Mscfld) Pwf (psi4 Forchheimer Backpressure 3.5 Horizontal Wells 49 4.5 Horizontal 2.6 Gas Density Because natural gas is compressible, its density depends upon pressure and temperature. Testing procedures include Flow-after-flow test, and Modified isochronal test. They referred to this effect as semi-infinite behavior because the rock matrix has infinite-acting characteristics. Economides, M. the temperature of the gas is very near that of the containing pipe and, as pipelines usually are buried, the temperature of the flowing gas is not influenced appreciably by rapid changes in atmospheric temperature of the flowing gas is not influenced appreciably by rapid changes in atmospheric temperature of the flowing gas is not influenced appreciably by rapid changes in atmospheric temperature of the flowing gas is not influenced appreciably by rapid changes in atmospheric temperature of the flowing gas is not influenced appreciably by rapid changes in atmospheric temperature of the flowing gas is not influenced appreciably by rapid changes in atmospheric temperature of the flowing gas is not influenced appreciably by rapid changes in atmospheric temperature of the flowing gas is not influenced appreciably by rapid changes in atmospheric temperature of the flowing gas is not influenced appreciably by rapid changes in atmospheric temperature of the flowing gas is not influenced appreciably by rapid changes in atmospheric temperature of the flowing gas is not influenced appreciably by rapid changes in atmospheric temperature of the flowing gas is not influenced appreciably by rapid changes in atmospheric temperature of the flowing gas is not influenced appreciably by rapid changes in atmospheric temperature of the flowing gas is not influenced appreciable (flowing gas is not i 1.49). All the spreadsheet programs are included on the CD included w ~ t hthis book. Major natural gas re\enres are found in the former Soviet Union, Middle East, Asia Pacific, Africa, North America, Southern and Central America, and Europe. Very often the z-factor is estimated with the chart developed by Standing and Katz (1942). Chapter 1 presents a brief introduction to the natural gas industry. Table 11-5 shows the solution of Example Problem 11.2 given by the spreadsheet. Chapter 7 focuses on the liquid separation process of natural gases. The equations are: P₁ = 2 S (f) D TY = AS₁, (11.71) where g p is based on pipeline imperfections such as initial out-ofroundness (ti,), eccentricit (usually neglected), and residual stress (usually neglected). The skin factor and non-Darcy coefficient can be estimated on the basis of pressure transient analyses. All of the wells were drilled and completed in essentially the same way, but there was still significant variation in gas to influence each other. This I S not only motivated by environmental considerations but also technological innovations and refinements. m.- (I) n 3,500 %' (I) 3.000 a 0 200 400 600 800 1,000 1,200 1.403 1,600 1.800 Gas Production Rate (Mscfld) Figure 3-2 IPR curves given by the spreadsheet program Empirical IPR.xls. Jenkins et al. One set of simple correlations is p,, = 709.604 - 58.7187, 16 Chapter 2 Properties of Natural Gas & OLFNWR9LHZ&DOFXODWLRQ([DPSOH Table 2-1 Compound Results Given by MixingRule.xlsa Yi 1.000 a. Flow within the fracture itself was not considered. 11.2.1.7.2 Pipelines in Parallel Consider a three-segment pipeline in parallel as depicted in Figure 11-2(b). mi 250 Chapter I I Transportation 11.2.2 Pipeline Wall Thickness Wall thickness design for steel pipelines is governed by U.S. Codes ASMEIANSI B32.8. Other codes such as 2187 (Canada), DnV (Norway), and IP6 (United Kingdom), have essentially the same requirements, but should be checked by the readers. - P w1f 2) This spreadsheet calculates and plots well IPR curve with empirical models. Coal-bed methane is the methane gas in minable coal beds with depths less than 3,000 ft. Solution The spreadsheet PseudoP.xls can be used for calculating real gas pseudopressure. All these codes can be used in other areas when no other code is available. Results are shown in Table 3-2. Input Data Reservoir pressure: 4,505 psia Test point 1, flow rate: 1,152 Mscfld bottom hole pressure: 3,025 psia 1,548 Mscfld Test point 2, flow rate: a. Chapters 3 through 6 co\ er in detail the performance of gas wells. Due to the low-permeability nature of shales, hydraulic fracturing is frequently needed to improve well productivity. Plot pressure: against pseudopressure in the pressure range from 14.7 psia to 10,000 psia. Unlike oil reserves that are mostly (80 percent) found in Organization of Petroleum Exporting Countries (OPEC), major natural gas reserves are found in the former Soviet Union, Middle East, Asia Pacific, Africa, North America, Southern and Central America, and Europe. Solution This problem is solved with the spreadsheet program Empirical Deliverability.xls. ASME 831.8 imposes Ph = 1.4 P, for offshore risers but allows onshore testing of prefabricated portions. The fine-grained rocks in the shale are micro-porous with extremely low permeabilities. The gas viscosity correlation of Carr, Kobayashi, and Burrows (1954) involves a two-step procedure: the gas viscosity at temperature and atmospheric pressure is estimated first from gas-specific gravity and inorganic compound content. Corrections for impurities in sour gases are always necessary. estimated using established correlations with confidence. Increasing the wall thickness can sometimes ensure hydrodynamic stabilization methods (e.g., weight coating). Dissolved gas is that portion of the gas dissolved in the crude oil and associated gas (sometimes called gas-cap gas) is free gas in contact with the crude oil. B.: Volumetric and Phase Behavior of Oil Field Hydrocarbon Systems. A reservoir is a porous and permeable underground formation containing an individual bank of hydrocarbon System. The results are presented in Appendix A. Natural gas provided close to 24 percent of U.S. energy sources over the three-year period 2000-02. Javadpour et al. On production, they may yield considerable quantities of hydrocarbon liquids. Demarchos, and L. An analyst expects shale gas to supply as much as half the natural gas production in North America by 2020 (Polczer, 2009). Isochronal testing sequence is shown in Figure 3-9. Table 2-5 shows data input and calculated parameters. The organic matter is believed to be an integral constituent of productive gas shale. The gas critical properties determined in such a way are called pseudocritical properties. The organic matter is believed to be an integral constituent of productive gas shale. processes of natural gases. The k f i i is fracture permeability in the near-wellbore region, and wWiis the width of the ith fracture in the near-wellbore region. The way to avoid such a crunch I S to expand energy supply and move from oil to natural gas and, eventually, to hydrogen. If ERW pipe is used, special inspection provisions such as full body ultrasonic testing are required. Traditionally, flow of gas in shale gas reservoirs was described using dual-porosity models that were originally developed for naturally fractured conventional reservoirs (Warren and Root, 1963; Streltsova, 1983). 7thed. Louisiana Department of Natural Resources. Example problems are illustrated and solved using computer programs provided with this book. When the two pressures p i and p2 lie in a region where z is essentially linear with pressure, then it is accurate enough to evaluate T at the average pressure p = (p l +p2)/2. The gas flow mechanism in the shale gas reservoirs is still not fully understood. Pipe types are: seamless, submerged arc welded (SAW or DSAW), electric resistance welded (ERW), and spiral welded. An efficiency factor ranging from 0.85 to 0.95 would represent a "clean" line. Carlson and Mercer (1991) pointed out that the behavior of gas flow in the shale matrix is different from that in conventional gas reservoirs due to desorption and diffusion effects. S ~ n c eits discovery in the United States in Fredonia, New York, in 182 1, natural gas has been used as fuel in areas immediately surrounding thc gas fields. Nonassociated gas is from reservoirs with minimal oil. For cases in which the wall thickness is based on Pd = Pi-PC, codes recommend not to overstrain the pipe. If expressed in rb/scf, it takes the form of 2.8 Compressibility of Natural Gas 27 Gas formation volume factor is frequently used in mathematical modeling of gas well inflow performance relationship (IPR). Figure 3-1 1 depict the technique for obtaining the A and B values from the isochronal test. C02 correction for gas viscosity at 14.7 psia: 0.000000 cp H2S correction for gas viscosity at 14.7 psia: 0.000000 cp Corrected gas viscosity at 14.7 psia (p,): 0.010504 cp Pseudoreducedtemperature: 1.45 This spreadsheet computes real gas pseudopressures. A general and more rigorous form of the Weymouth equation 2. ISBN 1-933762-41 1 (alk. The corrections can be made using either charts or correlations such as the WichertAziz (1972) corrected ppc) Tp, + B(I - B) E ~ Correlations with impurity corrections for mixture pseudocriticals are also available (Ahmed 1989) Applications of the pseudocritical pressure and temperature defined as: 2.4 Viscosity Gas viscosity is a measure of the resistance to flow exerted by the gas. They are future supplies beyond the proved reserves. It corresponds to the transition mode of collapse under external pressure (P,), axial tension (T,), and bending strain (gb) (Murphey and Langner 1985). 2.5 Compressibility Factor 25 Solution This problem is solved with the spreadsheet program HallYarborogh-z.xls. Considering gas flow from &OLFNWR9LHZ&DOFXODWLRQ([DPSOH Table 11-1 Input Data and Results Given by ~ i p e ~ a p a c i t ~. The first use of a similar process on a large scale outside the United States was the liquefaction by a refrigerative cycle of some of the resultant liquefied natural gas (LNG) by specially designed insulated tankers to Britain and France. Knowledge of these property values is essential for designing and analyzing natural gas, has had a long history in the United States, dating back about 80 years. This growth has resulted from several factors, including development of coal asymptic fuel for providing space and industrial process heat, use of natural gas in making petrochemicals and fertilizers, and strong demand for low-sulfur fuels. While natural gas engineering is well documented through many papers and sources, the computer applications that provide a crucial role in engineering design and analysis are not well published. An Energy White Paper. Most example calculations are presented with computer spreadsheets. The consumption of natural gas in all end-use classifications (residential, commercial, industrial, and power generation) has increased rapidly since World War 11. Even in the case of the highly mature and exploited United States, depending upon information sources, the potential remaining gas reserve estimates varies from 650 Tcf to 5,000 Tcf. 1.5 Types of Natural Gas Resources The natural gas, gas in tight shales, coal-bed methane, gas in geopressured reservoirs, and gas in gas hydrates. 3 . Figure 1-2 shows world energy consumption in the past three decades and forecast for the next two decades (DOEIEIA 2001). When the linear-radial flow model of Furui et al. Current production from conventional sources is not sufficient to satisfy all demands for natural gas. Houston: Gulf Publishing Company, 1989. Volumetric Measurement 11. The molecular weights of compounds (MW;) can be found in textbooks on organic chemistry or petroleum fluids such as that by McCain (1973). A light gas reservoir is one that contains primarily methane with some ethane. This correlation is summarized as follows: and where Y is the reduced density to be solved from If Newton-Raphson's iteration method is used to solve Equation (2.41) for Y, the following derivative is needed: Example Problem 2.4 For a natural gas with a specific gravity of 0.71, estimate z-factor at 5,000 psia and 180 O F. Example Problem 2.5 Natural gas from a gas reservoir has a specific gravity of 0.71. Unlike conventional gas reservoirs, where gas is stored in the open pore space of the rock, shales store a very large amount of gas in an adsorbed state (Shettler et al., 1987). The external pressure criteria should be based on nominal wall thickness, as the safety factors included in the following text account for wall variations. One can also use the arithmetic average of the z with 7 = (zl + z2)/2 where zl and z2 are obtained at p l and p2, respectively. Baton Rouge, January 201 1. As these functions are complicated and not explicit, a numerical integration technique is frequently used. 3 Panhandle A pipeline flow equation is thus where q i the gas flow rate in cfd measured at Tb and pb, and other terms are the same as in the Weymouth equation. This specific wellbore orientation allows multiple transverse fractures to be hydraulically created for enhancing productivity. Associated gas is the gas dissolved in oil under natural conditions in the oil reservoir. 3 Fracture linear flow in the fracture to the near-wellbore region. 1966): 997-1000. Also, T can be evaluated at an average pressure given by Regarding the assumption of horizontal, so that factors are needed in Equation (11.26) to compensate for changes in elevation. The appearance of the spreadsheet is shown in Table 3-7 and Table 3-8. 252 Chapter I I Transportation Most codes allow credit for external pressure. Demarchos, and P.E. Lewis. Definition of the compressibility factor is expressed as: z= 'actual h a 1 gas Introducing the z-factor to the gas law for ideal gas results in the gas law for real gas as: 2.5 Compressibility Factor 21 &OLFNWR9LHZ&DOFXODWLRQ([DPSOH Table 2-2 Results Given by Carr-Kobayashi-Burrows Viscosity.xlsa Input Data Pressure: 10,000 psia Temperature: Gas-specific gravity: 0.65 air = 1 Mole fraction of N2: 0.1 Mole fraction of N2: Devonian shales, the matrix is so tight that it takes a long time (many years) for the effects of a pressure drawdown in the fracture network to be felt deep in the interiors of the matrix. Includes b i b l i o g r a p h i c a l references and index. Standing, M. The model uses the effective wellbore radius (in radial flow) to simulate fluid flow toward the fractured well. rnput vata Pipe ID: 12.09 in Pipe roughness: 0.0006 in Pipeline length: 200 mi Average temperature: 60 OF 14.7 psia 600 psia 200 psia Base pressure: Inlet pressure: Outlet pressure: Gas properties: Gas-specific gravity: 0.7 air = 1 Mole fraction of N:, 0 Mole fraction of H2S: 0 Calculated Parameter Values Pseudocritical pressure: Pseudocritical temperature: 389.14 OR Uncorrected gas viscosity at 14.7 psia: 0.000000 cp C02 correction for gas viscosity at 14.7 psia: 0.000000 cp C02 correction psia (~1): Gas viscosity: Pseudoreduced pressure (psia): Pseud the Weymouth equation: Pipeline flow capacity: a. Brill, J. This spreadsheet calculates theoretical gas reservoir deliverability. For the outer region, the following well productivity model may apply: where where & and xf are the average half-distances between fractures and fracture half-length, respectively. Last but not least, our thanks are due to friends and colleagues too numerous to mention, who encouraged, assessed, and made poss~bleour editing this book. On the basis of their collective experience, we expect this book to be of value to engineers in the natural gas industry. Results are shown in Table 3-4. (201 1) pointed out that the role of formation damage in hydraulic fracturing shale gas wells is minimal, which is consistent with field observations that show that wells with high-water flowback volumes are unexpectedlj high-productivity wells. This is not only motivated by environmental considerations but also by technological innovations and refinements (Economides, Demarchos, Saputelli 2002). Of this, oil accounted for 39 percent, while natural gas and coal provided 23 percent, respectively (DOEEIA 2001). S. Special thanks go to the ChevronTexaco and American Petroleurn Institute (API) for providing ChevronTexaco Professorship and API Professorship in Petroleurn Engineering throughout the edition Dr.Boyun Guo and Dr.Ali Ghalambor University of Louisiana at Lafayette Houston, TX Natural Gas Engineering Handbook, 2nd Edition Copyright @ 20 12 by Gulf Publishing Company, Houston, Texas and D. Another approach is a volumetric appraisal of the potential undrilled areas. For greater diameters, the wall thickness for hydrotest condition. VDOC.PUB Authors: Guo, Boyun; Ghalambor, Ali PDF Download Embed This document was uploaded by our user. Appendix D presents charts for the minimum gas production rates for water removal in gas wells and Appendix E presents charts for the minimum gas production rates for condensate removal in gas well. "Computer Routine Treats Gas Viscosity as a Variable." in many parts of the world during the search for oil and gas. The nominal wall thickness should be determined such that: where 1.3 is the recommended safety factor on collapse, EB is the bending strain of buckling failure due to pure bending, and, gp is an imperfection parameter defined in the following text. 24 Chapter 2 Properties of Natural Gas Hall and Yarborough (1973) presented more accurate correlation to estimate z-factor of natural gas. This requires calculations involving flow in series, parallel, and series-parallel (looped) lines. L=10mi L1 = 7 mi L2 = 3 mi Dl = 4 i n D2 = 6 in increase in flow capacity 11.2 Pipeline Design 249 Similar problems can also be solved using the spreadsheet program LoopedLines.xls. It is believed that the first slope is determined by the permeability of the local fractures and combined stresses are sometimes limited by applicable codes and shall be checked for installation and operation. gives q = 1,653 Mscfld 2) Use Forchheimer equation with pressure-squared approach: Run Macro Solution to get result. The coefficients A and B are calculated from the two data points on stress-strain curve generated during a tensile test. / Component 1 Mole Fraction I Solution T h i s p r o b l e m i s solved w i t h t h e spreadsheet program MixingRule.xls. 30 Chapter 2 Properties of Natural Gas 0 1000 2.000 3000 4,000 5000 6000 7000 8 WO 9.000 10000 Pressure (ps~a) Figure 2-1 Plot of pseudopressures calculated by PseudoP.xls. Empirical models are therefore more attractive and widely employed in field applications. For H2S and C 0 2 contaminants, corrosion is often localized (pitting) and the rate of corrosion allowance ineffective. Brill and Beggs (1974) yield z-factor values accurate enough for many engineering calculations. Input Data T: 180 OF P: 5,000 psia SGFG. Jenkins et al.'s (2008) plot also shows a dual-slope behavior of gas wells. Reservoir temperature is 180 OF. Applying Equation (1 1.53) to the first two (parallel) segments gives: 11.2 Pipeline Design 245 r Figure 11-3 Sketch of looped pipeline. Table 3-6 Solution Given by Theoretical IPR.xls Pwr (psi4 q (Mscfld) p Approach p2 Approach Solution & OLFNWR9LHZ&DOFXODWLRQ([DPSOH 3.4 Construction of Inflow Performance Relationship Curve 45 & OLFNWR9LHZ&DOFXODWLRQ([DPSOH 3.4 Construction of Inflow Performance Relationship Curve 45 & OLFNWR9LHZ&DOFXODWLRQ([DPSOH 3.4 Construction of Inflow Performance Relationship Curve 45 & OLFNWR9LHZ&DOFXODWLRQ([DPSOH 3.4 Construction of Inflow Performance Relationship Curve 45 & OLFNWR9LHZ&DOFXODWLRQ([DPSOH 3.4 Construction of Inflow Performance Relationship Curve 45 & OLFNWR9LHZ&DOFXODWLRQ([DPSOH 3.4 Construction of Inflow Performance Relationship Curve 45 & OLFNWR9LHZ&DOFXODWLRQ([DPSOH 3.4 Construction of Inflow Performance Relationship Curve 45 & OLFNWR9LHZ&DOFXODWLRQ([DPSOH 3.4 Construction of Inflow Performance Relationship Curve 45 & OLFNWR9LHZ&DOFXODWLRQ([DPSOH 3.4 Construction of Inflow Performance Relationship Curve 45 & OLFNWR9LHZ&DOFXODWLRQ([DPSOH 3.4 Construction of Inflow Performance Relationship Curve 45 & OLFNWR9LHZ&DOFXODWLRQ([DPSOH 3.4 Construction of Inflow Performance Relationship Curve 45 & OLFNWR9LHZ&DOFXODWLRQ([DPSOH 3.4 Construction of Inflow Performance Relationship Curve 45 & OLFNWR9LHZ&DOFXODWLRQ([DPSOH 3.4 Construction of Inflow Performance Relationship Curve 45 & OLFNWR9LHZ&DOFXODWLRQ([DPSOH 3.4 Construction of Inflow Performance Relationship Curve 45 & OLFNWR9LHZ&DOFXODWLRQ([DPSOH 3.4 Construction of Inflow Performance Relationship Curve 45 & OLFNWR9LHZ&DOFXODWLRQ([DPSOH 3.4 Construction of Inflow Performance Relationship Curve 45 & OLFNWR9LHZ&DOFXODWLRQ([DPSOH 3.4 Construction of Inflow Performance Relationship Curve 45 & OLFNWR9LHZ&DOFXODWLRQ([DPSOH 3.4 Construction of Inflow Performance Relationship Curve 45 & OLFNWR9LHZ&DOFXODWLRQ([DPSOH 3.4 Construction of Inflow Performance Relationship Curve 45 & OLFNWR9LHZ&DOFXODWLRQ([DPSOH 3.4 Construction of Inflow Performance Relationship Curve 45 & OLFNWR Table 3-6 Solution Given by Theoretical IPR.xls (Continued) Pwr ( q (Mscfld) p Approach Example Problem 3.2 with both Forchheimer and backpressure equations. It also contains the following compounds: I Mole fraction of N,: 1 0.10 1 I Mole fraction of Approach Example Problem 3.2 with both Forchheimer and backpressure equations. It also contains the following compounds: I Mole fraction of N,: 1 0.10 1 I Mole fraction of Approach Example Problem 3.2 with both Forchheimer and backpressure equations. It also contains the following compounds: I Mole fraction of N,: 1 0.10 1 I Mole fraction of Approach Example Problem 3.2 with both Forchheimer and backpressure equations. It also contains the following compounds: I Mole fraction of N,: 1 0.10 1 I Mole fraction of Approach Example Problem 3.4 Construct IPR curve for the well specified in Example Problem 3.4 Construct IPR curve for the well specified in Example Problem 3.4 Construct IPR curve for the well specified in Example Problem 3.4 Construct IPR curve for the well specified in Example Problem 3.4 Construct IPR curve for the well specified in Example Problem 3.4 Construct IPR curve for the well specified in Example Problem 3.4 Construct IPR curve for the well specified in Example Problem 3.4 Construct IPR curve for the well specified in Example Problem 3.4 Construct IPR curve for the well specified in Example Problem 3.4 Construct IPR curve for the well specified in Example Problem 3.4 Construct IPR curve for the well specified in Example Problem 3.4 Construct IPR curve for the well specified in Example Problem 3.4 Construct IPR curve for the well specified in Example Problem 3.4 Construct IPR curve for the well specified in Example Problem 3.4 Construct IPR curve for the well specified in Example Problem 3.4 Construct IPR curve for the well specified in Example Problem 3.4 Construct IPR curve for the well specified in Example Problem 3.4 Construct IPR curve for the well specified in Example Problem 3.4 Construct IPR curve for the well specified in CO,: 0.08 I Mole fraction of H2S: 0.02 Calculate pseudopressure at 10,000 psia and 180 O F. Although they occur as gases in underground reservoirs, they have a high content of hydrocarbon liquids. Example Problem 1 1.2 Consider a 4-in pipeline that is 10 miles long. p. Some of the codes are ASME B3 1.8 (no limit on hoop stress during hydrotest) and DnV [Clause 8.8.4.31. Except in specific cases, only seamless or SAW pipe are to be used, with seamless being the preference for diameters of 12 inches or less. !%! and real gas law, p = p(MW)a - zRT, Weymouth (19121 developed zRT the following equation: where e = 2.7 18 and and & is equal to outlet elevation minus inlet elevation (note that & is positive when outlet is higher than inlet). The use of refrigeration to liquefy natural gas, and helice reduce its volume to the point where it becomes economically attractive to transport across oceans by tanker, was first attempted on a small scale In Hungary in 1934 and later used in the United States for moving gas in liquid form from the gas. fields in Louisiana up the Mississippi River to Chicago in 1951 (Ikoku 1984). viil Contents 10.2.4 Selection of Orifice Meter 212 10.3.1 Displacement Metering 212 10.3.2 Turbine Meter 214 10.3.3 Elbow Meter 214 10.4 Natural Gas Liquid Measurement 215 11 Transportation .263 12.1 Introduction 263 12.2 Liquid Loading on Gas Wells 263 12.2.1 Turner's Method 264 12.2.2 Guo's Method 267 12.2.3 Comparison of Methods 273 12.2.4 Solutions to the Liquid Loading Problem 275 12.3.1 Hydrate Formation 281 12.4 Pipeline Cleaning 287 12.4.2 Selection of Pigs 298 12.4.3 Major Applications 306 12.4.4 Pigging .. You're Reading a Free Preview Pages 4 to 5 are not shown in this preview. Note: In certain cases, it may be desirable to order a nonstandard wall. Gas density can be calculated from gas law for real gas with good accuracy: where m is mass of gas and p i s gas density. Louisianc~Energy Facts. Assuming a Darcy skin factor of 5 and a non-Darcy coefficient of 0.001 day/Mscf, estimate the deliverability of the gas reservoir under pseudosteady state flow condition at a flowing bottom hole pressure of 3,000 psia. On the other hand, should pl and p2 lie in the range where z is not linear with pressure (double-hatched lines), the proper average would result from determining the area under the z-curve and dividing it by the difference in pressure: where the numerator can be evaluated numerically. It is a historical imperative that the transition from oil to natural must be made in the early twenty-first century. (10'3 Btu. The inorganic compounds nitrogen, carbon dioxide, and hydrogen sulfide are not desirable because thcy are not combustible and cause corrosion and other problems in gas production 81 5.2 Sonic and Subsonic Flow 81 5.3 Dry Gas Flow through Chokes 82 5.3.1 Subsonic Flow 82 5.3.2 Sonic Flow 85 5.3.3 Temperature at Choke 85 5.3.4 Applications 86 5.4 Wet Gas Flow through Chokes 92 6 Well Deliverability Figure 3-3 shows two regions of the reservoir. (I) %' a -w I 0 500 1.000 1.500 2,000 2.500 Gas Production Rate (Mscfld) Figure 3-IPR curves given by the spreadsheet program Theoretical IPR.xls. Transportation 12. mile (Jenkins et al., 2008) 3.8.1 Flow-After-Flow Test In this testing procedure, a well flows at a selected constant rate until pressure stabilizes to reach the pseudosteady state flow condition. Even in the case of the highly mature and exploited United States depending upon information sources, the potential remaining gas reserve estimates vary from 650 Tcf to 5,000 Tcf (Economides et al. cm. &OLFNWR9LHZ&DOFXODWLRQ([DPSOH Table 2-3 Results Given by Brill-Beggs-Z.xIsa Input Data Pressure: 5,000 psia Temperature: 180 OF Gas-specific gravity: 0.65 1 for air Mole fraction of N2: 0.1 Mole fracting fraction of N2: 0.1 Mole fraction of N2: 0.1 Mole fracti fraction of C02: 0.08 Mole fraction of H2S: 0.02 Calculated Parameter Values a. 238 Chapter 11 Transportation 11.2.1.5.4 Panhandle B equation for long transmission and delivery lines. Dean, D. N o part of this publication may be reproduced or transmitted in any form without the prior written permission of the publisher. Chapter 9 presents principles of gas conlpression and cooling. Potential resources constitute those quantities of natural gas that are believed to exist in various rocks of the Earth's crust but have not yet been found by the drill. U. Different limiting assumptions have been made, such as drilling depths, water depths in offshore areas, economics, and technological factors. 00 Text design and composition by TIPS Technical Publishing, Inc. The temperature derating factor (F,) is equal to 1.0 for temperatures under 250 OF. Table 3 4 Results Given by Empirical Deliverability.xls & OLFNWR9LHZ&DOFXODWLRQ([DPSOH Solution 1) Use Forchheimer equation with real gas pseudopressure at pressure 3,025 psia: 588,157,460 psi2/cp Enter real gas pseudopressure at pressure 1,685 psia: 198,040,416 psi2/cp Enter real gas pseudopressure at the desired pressure at the desired pressure 1,050 psia: 79,585,534 psi2/cp 42 Chapter 3 Gas Reservoir Deliverability &OLFNWR9LHZ&DOFXODWLRQ([DPSOH Table 3 4 Results Given by Empirical Deliverability.xls (Continued) A = [m (p)- m(pwf11) 2 - B41 = 208,000 41 Run Macro Solution to get result. An isochronal test is conducted by flowing a well at a fixed rate, then shutting it in until the pressure builds up to an unchanging value. 248 Chapter 11 Transportation = 1.1668, or 16.68% increase in flow capacity (b) This problem can be solved with Equation (11.54). At the end of the last century, natural gas took over the position of coal as the number two energy source behind oil. As the real gas pseudopressure is difficult to evaluate without a computer program, approximations to Equation (3.1) are usually used in the natural gas industry. (3.8) 41 n = (3.9) (3.10) Similar to Equation (3.1), Equation (3.5) and Equation (3.1), Equatio q241 (3.13) 40 Chapter 3 Gas Reservoir Deliverability (P2 - Ptf1) - B912 (3.14) A = 91 n = C = (3.15) 2 91 (3.16) [u2 - Pij,] "Example Problem 3.2 A gas well produces 0.65 specific gravity natural gas with N2, COP, and H2S of mole fractions 0.1, 0.08, and 0.02, respectively. IPR curves are shown in Figure 3-1. However, X-65 steel can be used if the ductility is kept high by selecting the proper steel chemistry and micro alloying. It is clear that natural gas is now becoming the premier fuel of choice for the world economy. What is your conclusion? 11.2.1.7.1 Pipelines in Series Consider a three-segment pipeline in a series of total length L depicted in Figure 11-2(a). c. Dempsey, J. New York: McGrawHill, 1980. This book can also be used as a reference tor college students of undergraduate levels in petroleum engineering. Houston: Simmons and Company International, October 2000. Baton Rouge, March 201 1. In 2000, total world energy consumption was slightly below 400 quadrillion 8 Chapter 1 Introduction -Natural ---1970 1975 gas Nuclear Other 1980 1985 1990 1995 2000 2005 2010 2015 2020 Year Figure 1-2 World energy in all sectors of the economy. 2-3 For a 0.65 specific gravity gas at 250 OF, calculate and plot pseudopressures in a pressure range from 14.7 psia and 8,000 psia. Pseudopressure values in the whole range of pressure are plotted in Figure 2-1. Bai (2001) presents a Design Through Analysis (DTA) method. The uploader already confirmed that they had the permission to publish it. 0.71 air = 1 Calculate Critical and Reduced Temperature and Pressure Tpc = 1.632902995 t = 1TTpr: 0.61240625 Ppr = p/Ppc: 7.487462244 Calculate Temperature dependentTerms Calculate Reduced Density (use Macro Solution) Y = ASSUMED: 0.239916681 Calculate z-Factor a. 46 Chapter 3 Gas Reservoir Deliverability - Pressure - n Approach (I) ? Appendix B provides charts for determining normalized pressures of sweet natural gases. Using the Weymouth equation: To speed up trial-and-error calculations, a spreadsheet program, PipeCapacity.xls, was developed. The atmospheric pressure viscosity (pl)can be expressed as: where , LL, ~ = $8.188 \times -6.15 \times 10 \sim (\sim,) + (1 \cdot where n is the number of moles of gas.$ 14.7 psia: 0.012174 cp N2 correction for gas viscosity at 14.7 psia: 0.000800 cp CO, corrected gas viscosity at 14.7 psia: 0.000043 cp Corrected g spreadsheet calculates gas viscosity with correlation (10' 3 Btu. Natural ga\i \ a subcategory of petroleum that is a naturally occurring, complex n~ixture f hydrocarbons, with a minor amount of inorganic compound\. A common economical solution to these problems is to place one or more lines in parallel, either partially or throughout the whole length, or to replace a portion of the line with a larger one. Because gas hydrate is a highly concentrated form of natural gas and extensive deposits of naturally occurring gas hydrates have been found in various regions of the world, they are considered as a future, unconventional resource of natural gas. D., Jr. The Properties of Petroleum Fluids, Tulsa: PennWell Books, 1973. Applying the Weymouth equation (1 1.52) gives: Dividing Equation (1 1.53) by Equation (1 1.50) yields: 11.2.1.7.3 Looped Pipelines Consider a three-segment looped pipeline depicted in Figure 11-3. The problem with the term "dual-porosity" in shales, however, is that shales have very little open porosity. In the spreadsheet, gas viscosity is calculated with the correlation of Carr, Kobayashi, and Burrows. Table 11-6 Design and Hydrostatic Pressure Definitions and Usage Factors for Gas Lines ASME B31.8 1989 Edition 1990 Addendum DnV 1981 pi- P, [4.2.2.2] 77 for pipeline 0.72 [4.2.2.1] 7 for riser sections(b) 0.5 [4.2.2.1] 7 for riser sections(b) 0.5 [4.2.2.1] 7 for pipeline 0.72 [4.2.2.1] 7 natural gas reserves. Gases in tight sands are found in many areas that contain formations generally having porosities of 0.001 to 1 millidarcy (md). Cieologists and chemists agree that petroleum originates from plants and a n ~ m a remains l that accumulate on the seallake floor along with the sedimentary rocks. "A New Equation of State for ZFactor Calculations." Oil & Gas Journal (June 18, 1973): 89. Ikoku, C. This chapter presents methods that can be used for establishing gas well IPR under different flow conditions. The appearance of the spreadsheet is shown in Table 3-5 and Table 3-6. Simmons, M. The safety factor on collapse is calculated for D/t ratios along with the loads (Pe&,Ta) and initial pipeline out-of-roundness (6,). 16, 1965): 141. This issue of correction for change in elevation is addressed in the next section. 1.6 Future of the Natural Gas Industry 5 0 25000 & 5 0 F 20000 u 2 n -d 2 ? According to Katsube (2000), gas flows through a network of pores with different diameters ranging from nanometres (nm = 10-ym)to micrometres (pm = 10-m) More specifically, the diameter of pores in shale gas sediments ranges from a few manometres to a few manometres to a few manometres (nm = 10-ym)to micrometres shows that wall allowance is only one of several methods available to prevent corrosion, and often the least recommended. Lee, A. CD-ROMs I.Ghalambor, A l i . In a rapidly subsiding basin area, clays often seal underlying formations and trap their contained fluids. on gas viscosity and compressibility factor, which are properties of the gas. Guo et al. 2 Calculate the minimum wall thickness required to withstand external pressure. Core analysis has determined that the shale itself may have up to 12 percent porosity, however, permeability values are commonly less than 1 md. 58 Chapter 3 Gas Reservoir Deliverability Figure 3-6 - Pwf Sequence of flow-after-flow test 100 q, 3.8 Well Deliverability Testing 59 o Recorded data 2 Point on line Figure 3-7 AOF Technique for deriving the A and B values from flow-after-flow test 100 q, 3.8 Well Deliverability Testing 59 o Recorded data 2 Point on line A pwf=14.7 psi 1 10 Figure 3-7 AOF Technique for deriving the A and B values from flow-after-flow test 100 q, 3.8 Well Deliverability Testing 59 o Recorded data 2 Point on line Figure 3-8 Technique for deriving the A and B values from flow-after-flow test 100 q, 3.8 Well Deliverability Testing 59 o Recorded data 2 Point on line A pwf=14.7 psi 1 10 Figure 3-7 AOF Technique for deriving the A and B values from flow-after-flow test 100 q, 3.8 Well Deliverability Testing 59 o Recorded data 2 Point on line A pwf=14.7 psi 1 10 Figure 3-8 Technique for deriving the A and B values from flow-after-flow test 100 q, 3.8 Well Deliverability Testing 59 o Recorded data 2 Point on line A pwf=14.7 psi 1 10 Figure 3-8 Technique for deriving the A and B values from flow-after-flow test 100 q, 3.8 Well Deliverability Testing 59 o Recorded data 2 Point on line A pwf=14.7 psi 1 10 Figure 3-8 Technique for deriving the A and B values from flow-after-flow test 100 q, 3.8 Well Deliverability Testing 59 o Recorded data 2 Point on line A pwf=14.7 psi 1 10 Figure 3-8 Technique for deriving the A and B values from flow-after-flow test 100 q, 3.8 Well Deliverability Testing 59 o Recorded data 2 Point on line A pwf=14.7 psi 1 10 Figure 3-8 Technique for deriving the A and B values from flow-after-flow test 100 q, 3.8 Well Deliverability Testing 59 o Recorded data 2 Point on line A pwf=14.7 psi 1 10 Figure 3-8 Technique for deriving the A and B values from flow-after-flow test 100 q, 3.8 Well Deliverability Testing 59 o 3.8.2 Isochronal Test The isochronal testing procedure was developed to obtain data with reduced test time. Dl = 4 in D2 = 6 in %-416/3 + 616/3 = 3.9483, or 294.83% increase in flow 41 capacity (c) This problem can be solved with Equation (11.61). A similar type of problem may arise when an existing pipeline must be "pressure derated" because of age (corrosion, etc.) but this pipeline is desired to maintain the same throughput. Sloan, E. Preface It is well recopnized that the nineteenth century was a century of coal that supported the Initiation of industrial revolution in Europe. The results are presented in Appendix B. The transmission factor has long been the most difficult to evaluate. 3 Add wall thickness allowance for corrosion, if applicable, to the maximum of the preceeding. However, these criteria are not normally used for wall thickness determination. The model incorporates linear flow within the fractures, radial flow within the fractures to the horizontal wellbore, and flow from the fractured region directly to the horizontal wellbore. The compressibility of the fluid can be considered constant and an average effective gas deviation factor may be used. Clathrate Hydrates of Natural Gases. To counter any deficiency that might arise from the limitations of space, we provide a reference list of books and papers at Preface xiii the end of cach chapter so that readers should experience little difficulty in pursuing each topic beyond the presented scope. Louisianu Energy Facts. (2008) presented cumulative gas production data for 23 wells in a I-sq mile area. Consequently, gas production at that time was often short-lived, and gas could be purchased as low as 1 or 2 cents per 1,000 cu ft in the field (Ikoku 1984). The consutnpt ion of natural gas in all end-use classifications (residential, commercial, industrial, and power generation) has increased rapidly since World War 11. 8 5 ~lod kfiiw, (p: - p\$) 4 =1=12 + n - (1.224 - s, - Dq) 1 where pwl is the flowing bottom-hole pressure. The contributing factors are thought to be bacterial action; shearing pressure during compaction, heat, and natural distillation at depth; possible addit~onof hydrogen from deep-seated sources; presence of catalysts; and t ~ m c(Allison and Palmer 1980). The result is shown in Table 2-4. (2008) suggests that the following modified Joshi equation be applied to gas wells: where and qg= gas production rate (Mscflday) kH = the average horizontal permeability (md) r, = \sim radius of drainage area of horizontal well (ft) L = length of horizontal well (r, L = length of horizontal well) r, = \sim radius of drainage area of horizontal well (r, L = length of horizontal well) r, = \sim radius of drainage area of horizontal well (r, L = length of horizontal well) r, = \sim radius of drainage area of horizontal well (r, L = length of horizontal well) r, = \sim radius of drainage area of horizontal well (r, L = length of horizontal well) r, = \sim radius of drainage area of horizontal well (r, L = length of horizontal well) r, = \sim radius of drainage area of horizontal well (r, L = length of horizontal well) r, = \sim radius of drainage area of horizontal well (r, L = length of horizontal well) r, = \sim radius of drainage area of horizontal well (r, L = length of horizontal well) r, = \sim radius of drainage area of horizontal well (r, L = length of horizontal well) r, = \sim radius of drainage area of horizontal well (r, L = length of horizontal well) r, = \sim radius of drainage area of horizontal well (r, L = length of horizontal well) r, = \sim radius of drainage area of horizontal well (r, L = length of horizontal well) r, = \sim radius of drainage area of horizontal well (r, L = length of horizontal well) r, = \sim radius of drainage area of horizontal well (r, L = length of horizontal well) r, = \sim radius of drainage area of horizontal well (r, L = length of horizontal well) r, = \sim radius of drainage area of horizontal well (r, L = length of horizontal well) r, = \sim radius of drainage area of horizontal well (r, L = length of horizontal well) r, = \sim radius of drainage area of horizontal well (r, L = length of horizontal well) r, = \sim radius of horizontal well (r, L = length of horizontal well) r, = \sim radius of horizontal well (r, L = length of horizontal well) r, = \sim radius of horizontal well (r, L = length of horizontal well) r, = \sim radius of horizontal well (r, L = length of horizontal well) = average gas compressibility factor (dimensionless) b = skin factor (dimensionless) b = skin factor (dimensionless) b = NON-Darcy flow coefficient (day/Mscf) The method for obtaining the correction factor Fg was given by Guo et al. tinder what condition is the pseudopressure linearly proportional to pressure? The well diameter is 7-718 inches. Gas Reservoir Deliverability 4. At pressures lower than 2,000 psia, where pb is the base pressure, ,Z is the average gas viscosity, and i is the average gas compressibility factor. Report DMCA The demand for energy consumption is increasing rapidly. Gas shales are essentially lithified clays with organic matter present in varying amounts. This book I S based on numerous documents including reports and papers accumu1atc.d through many years of work at the University of Louisiana at Lafayette. 2-4 Prove that the compressibility 3.1 Introduction Gas reservoir deliverability is evaluated using well inflow performance relationship (IPR). It is generally economical to design for propagation pressure for diameters less than 16 inches. = 709 Mscfld 4 = [= 759 Mscfld o yr e] + s + D g] 1 4 1. Proved natural gas reserves in 2000 were about 1,050 Tcf in the United States and 170 Tcf in Canada. Chapter 10 describes gas-metering techniques. Its value reflects how much the real gas deviates from the ideal gas at given pressure and temperature. Most fractured horizontal wells are drilled in low-permeability reservoirs, in which fluid flow from the unfractured region, and the outer region is the non-fractured region (Guo et a]., 2008). Two commonly used empirical models are the Forchheimer model and hackpressure model. "Viscosity of Hydrocarbon Gases under Pressure." Trans.AIME 201 (1954): 264-72. DnV is for oil, gas, and two-phase flow pipelines in the North Sea. b. ASME B31.8 is for all gas lines and two-phase flowlines in North America. Numerical integration is performed with a trapezoidal method. Assuming that the compression and delivery pressures will maintain unchanged, calculate gas capacity increases by using the following measures of improvement: (a) Replace three miles of the 4-in pipeline by a 6-in pipeline segment; (b) Place a 6-in parallel pipeline to share gas transmission; and (c) Loop three miles of the 4-in pipeline with a 6-in pipeline segment. Higher grades can be selected in special cases. (1991) to include the effect of reservoir anisotropy. Shale gas has become an increasingly important source of natural gas in several regions of the world over the past decade. &OLFNWR9LHZ&DOFXODWLRQ([DPSOH Table 3-1 The First Section of Theoretical Deliverability.xlsa Instructions: 1) Go to the Solution and view results. Table 1 1 4 Constants for Empirical Pipeline Flow Equations Equation a1 a2 a3 a4 a5 433.5 1 0.5 0.5 2.667 Panhandle A 435.87 1.0788 0.5394 0.4604 2.618 Panhandle B 737 1.02 0.51 0.49 2.53 Weymouth 11.2.1.7 Series, Parallel, and Looped Pipelines It is often desirable to increase the throughput of an existing pipeline by gathering gas from new gas wells. Proved natural gas reserves in 2000 are about 1,050 Tcf in the Unltes States and 170 Tcf in Canada. It has been noted that bending loads have no demonstrated influence on the propagation pressure. Hall, K. It is normally used for estimating gas reserves. Chapter 12 deals with special problems in natural gas production operations. Gas deviation factor is calculated with the correlation of Brill and Beggs. Wellbore Performance 5. The molecular weight of air is usually taken as equal to 28.97 (approximately 79% nitrogen and 21% oxygen). Table 11-3 presents some transmission factors that are the most significant and have either best stood the test of usage or have strong foundations in basic flow theories. xl s (~) Instructions: 1) Update input data; 2) Run Macro Solution and view results. Alternatively, it can be stored for future use in insulated tanks or subsurface storages. Example Problem 1.1 Natural gas from the Schleicher County, Texas, Straw Reef has a heating value of 1,598 Btulscf. If this gas is used to generate electricity at a rate of 1 MMscfIday, how many watts of electricity would the generator produce if the overall efficiency is 50% (1 hp = 745 W)? A11 crude oil reservoirs contain dissolved gas and may or may not contain associated gas. He concluded that when the semi-infinite flow prevails, the performance of the singlewell system depends on fracture permeability, the external drainage radius, and a group of parameters including matrix properties, fluid viscosity, and fracture spacing. Empirical models of gas discoveries and production have also been developed and converted to mathematical models. 6 Check for handling is difficult for D/r larger than 50; welding of wall thickness less than 0.3 in (7.6 mm) requires special provisions. Gas well IPR determines gas production rate as a nonlinear function of pressure drawdown (reservoir pressure). Brill and Beggs' z-factor correlation is expressed as follows: and 2.5 Compressibility Factor 23 Example Problem 2.2, estimate z-factor at 5,000 psia and 180 O F. xii Preface Natural gas engineering has supported the natural gas and coal provided 23 percent, respectively. point 1 to point 2 in a nonhorizontal pipe, the first law of thermal dynamics gives: Based on the pressure gradient due to the weight of gas column -? The theoretical background is not given in this book. "Energy Sources and Energy Intensity for the Twenty-First Century." Paper SPE 75504 presented at the SPE Gas Technology Symposium, Calgary, Alberta, Canada, April 30-May 2, 2002. Simmons (2000) concluded that energy disruptions should be a "genuine concern." Simmons suggests that it will likely cause chronic energy shortage as early as 2010. The very conservative estimates (DOEEIA 2001) suggest that while the total annual energy demand between 2000 and 2020 will increase by 30 percent from 98 to 127 quadrillion Btu, natural gas will increase by over 60 percent from 22.5 to 35.6 quadrillion Btu, or about 35 Tcf. It is a historical imperative that the transition from oil to natural gas must be made in the early twenty-first century. After further subsidence, the pressure and temperature of the transition from oil to natural gas must be made in the early twenty-first century.

can be selected for low-pressure, large diameter pipelines to reduce material cost, or in cases that require high ductility for improved impact resistance. which are valid for H2S < 3%, N2 < 5%, and total content of inorganic compounds less than 7%. to account for head of fluid and for lines that traverse from deep to shallow water. Example Problem 3.3 Construct IPR curve for the well specified in Example Problem 3.1 with both pressure and pressure-squared approaches. The assumption is justified for work with commercial transmission lines. during fabrication, transportation, and storage. Quantities of gas can be stored either as a dissolved phase in liquid hydrocarbons, or as an adsorbed phase on other materials within the shales of the kerogen, i.e., certain forms of illite. When one standard cubic feet of natural gas is combusted, it generates 700 Btu to 1,600 Btu 1.2 Utilization of Natural Gas 3 of heat, depending upon gas composition. i 15000 loo00 u 34 5000 3 0 1920 1930 1940 1950 1960 1970 1980 1990 2000 2010 Figure 1-3 U.S. natural gas production history (Louisiana Department of Natural Resources 2011). Following the sequence of natural gas production, i this book presents its contents in twelve chapters. 2.9 Real Gas Pseudopressure 29 & OLFNWR9LHZ&DOFXODWLRQ([DPSOH Table 2-5 Input Data and Calculated Parameters Given by PseudoP.xlsa Input Data .- Base pressure: 10,000 psia Temperature: -- Gas-specific gravity: 0.6 1 for air Mole fraction of N2: 0 Mole fraction of H2S: 0 Calculated Parameter Values Pseudocritical pressure: 673 psia - Pseudocritical temperature: 357.57 OR - Uncorrected gas viscosity at 14.7 psia: 0.010504 cp - N2 correction for gas viscosity at 14.7 psia: 0.010504 cp - N2 correction for gas viscosity at 14.7 psia: 0.010504 cp - N2 corrected gas viscosity at 14.7 psia: 0.010504 cp - N2 correction for gas viscosity at 14.7 psia: 0.010504 cp - N2 corrected g compared to the fractured region of the reservoir. Figure 3-4 illustrates flow in the fracture. 11.2.1.6 Practical Pipeline Equations were developed for perfectly clean lines filled with gas. This book fills the gap. Solution Output power of the generator: 1,000 kW = (1,000 kW)(3,412 Btulh per kW) 4 Chapter 1 Introduction Fuel gas requirement: (8.19 x lo7 Btulday)/(1,598 Btu/scf)/(0.5) = 1.025 x lo5 scflday = 102.5 Mscflday 1.3 Natural Gas Industry Natury Natural Gas Industry Natural Gas Indu particularly as a nonpolluting fuel for aircraft and ground vehicles. A rich or heavy gas reservoir may hale a gravity equal to 0.75 or, in some rare cases, higher than 0.9. 2.3 Pseudocritical properties of a gas can be determined on the basis of the critical properties of compounds in the gas using the mixing rule. Assume that the overall efficiency is 50 percent (1 kW =: 3.412 Btulh). There are often scales and even " j u n k left in the line. The nominal pressure defined as the difference between the internal pressure (Pi) and external pressure (P,); D is nominal outside diameter; t, is thickness allowance for corrosion; and, ayis the specified minimum yield strength. Gas wells are wells with producing gas-oil-ratio (GOR) being greater than 100,000 scflstb; 2 Chapter I Introduction Table 1-1 I Composition of a Typical Natural Gas Compound I I Methane Mole Fraction 0.8407 I Ethane 0.0586 I propane I 0.0220 I Hexane 0.0028 1 / 1 -1 and Heavier 1 Carbon Dioxide 1 Hydrogen Sulfide I 0.0063 I Nitrogen 0.0345 Total 1.0000 -\$ condensate wells are those with producing GOR being less than 5.000 scflstb but greater than 5.000 scflstb but greater than 5.000 scflstb. slope, Le is defined as For a nonunithrm slope (where elevation change cannot be simplified to a single section of constant gradient), an approach in steps to any number of sections, n, will yield where 11.2.15. Both the back pressure model and the Forchheimer model can be used to analyze the test data. 2020 9 10 Chapter I Introduction 1.7 References Allison, I. If gas composition and viscosity is very often estimated with charts or correlations developed based on the charts. Taking air molecular weight 29 and R = 10.73 psia - ft3 mole - " R , Equation (2.43) is rearranged to yield: where the gas density is in lbm/ft3. Combining Equations (3.19) through (3.22) yields a reservoir deliverability 3.7 Shale Gas Wells Shale gas is natural gas produced from shale sequences. The twentieth century of oil that was the primary energy source to support the growth of global economy. 232 Chapter 11 Transportation Example Problem 1 1.1 For the following data given for a horizontal pipeline, predict gas is found with crude oil. "Natural Gas: Beyond All Expectations." Paper SPE 7 15 12 presented at the 2001 SPE Annual Technical Conference and Exhibition, New Orleans, Louisiana, September 30-October 3, 2001. Society of a singlediameter (D3)pipeline is expressed as: Dividing Equation (11.60) yields: Let Y be the fraction of looped pipeline and X be the increase in gas capacity, Equation (11.61) can be rearranged as: where RD is ratio of the looping pipe diameter to the original pipe diameter. gas. Compression and Cooling 10. If possible, the final flow period should be long enough to achieve stabilized flow condition. (2007) presented experimentally obtained permeabilities of 152 samples from nine shale gas reservoirs with pore- 3.7 Shale Gas Wells 55 size distribution of several shale samples at 60,000 psi mercury injection pressure. Some estimates were based on growth curves, extrapolations of past productivity of gas wells. A pool contains one or more resen oirs in isolated structures. The efficiency factor expresses the actual flow capacity as a fraction of the theoretical flow rate. 1,528 Mscfld bottom hole pressure 3,025 psia Test point 1, flow rate: 1,548 Mscfld bottom hole pressure 1,685 psia Solution log[\$) n= 2 p2 - Pwf 1 l o g [P2 a. 11.2 Pipeline Design 23 1 The heat of compression is usually dissipated into the ground along a pipeline within a few miles downstream from the compressor station. The result is shown in Table 2-2. This must-have handbook includes: A focus on real-world needs rather than theoryIllustrative examples throughout the textSpreadsheet programs for all the engineering calculations Exercise problems at the end of every chapter, including newly added questions covering today's technologies, such as multi-fractured horizontal wells and shale gas wellsContent: Front Matter • List of Spreadsheet Programs Spreadsheet Programs and Functions • List of Nomenclature • Preface • Table of Contents 1. Palmer. 3.8 0 10 20 30 Well Deliverability Testing 40 50 60 70 57 80 T i m e (months) Figure 3-5 Gas production curves of 3 wells in a 1-sq. Natural gas is the only fuel that is superior to other energy sources in economic attractiveness and environmental concerns. The philosophy involved in deriving the special relationships used in the solution of complex transmission systems as equivalent lengths of common diameter of a common length, there equivalent means that both lines will have the same capacity with the same totally pressure drop. At the receiving terminals, the LNG is reconverted to a gaseous state by passage through a regasifying plant, whence it can be fed as required into the normal gas distribution grid of the importing country. (2005) published a comprehensive description of pipeline design, installation, and operations for offshore and deepwater development. B. Input Data Effective permeability to gas: 0.17 md Pay zone thickness: 78 ft Equivalent drainage radius: 0.022 cp The average gas compressibility to gas: 0.17 md Pay zone thickness: 78 ft Equivalent drainage radius: 0.021 cp The average gas compressibility to gas: 0.17 md Pay zone thickness: 78 ft Equivalent drainage radius: 0.021 cp The average gas compressibility to gas: 0.17 md Pay zone thickness: 78 ft Equivalent drainage radius: 0.022 cp The average gas compressibility to gas: 0.17 md Pay zone thickness: 78 ft Equivalent drainage radius: 0.021 cp The average gas compressibility to gas: 0.17 md Pay zone thickness: 78 ft Equivalent drainage radius: 0.021 cp The average gas compressibility to gas: 0.17 md Pay zone thickness: 78 ft Equivalent drainage radius: 0.021 cp The average gas compressibility to gas: 0.17 md Pay zone thickness: 78 ft Equivalent drainage radius: 0.021 cp The average gas compressibility to gas: 0.17 md Pay zone thickness: 78 ft Equivalent drainage radius: 0.021 cp The average gas compressibility to gas: 0.17 md Pay zone thickness: 78 ft Equivalent drainage radius: 0.021 cp The average gas compressibility to gas: 0.17 md Pay zone thickness: 78 ft Equivalent drainage radius: 0.021 cp The average gas compressibility to gas: 0.17 md Pay zone thickness: 78 ft Equivalent drainage radius: 0.021 cp The average gas compressibility to gas: 0.17 md Pay zone thickness: 78 ft Equivalent drainage radius: 0.021 cp The average gas compressibility to gas: 0.17 md Pay zone thickness: 78 ft Equivalent drainage radius: 0.021 cp The average gas compressibility to gas: 0.17 md Pay zone thickness: 78 ft Equivalent drainage radius: 0.021 cp The average gas compressibility to gas: 0.17 md Pay zone thickness: 0.17 md Pay zone thi factor: Effective permeability to gas: a. MWi y i ~ ~ Pci i MW, = 20.71 y, = 0.71 (psia) YiPci ("R) ppc= 661 Tpc = 41 1 Tci This spreadsheet calculates gas apparent molecular weight, specific gravity, pseudocritical pressure, and pseudocritical temperature. Spiral weld pipe is very unusual for gas pipelines and should be used only for low-pressure water or outfall lines. Properties of Natural Gas 3. Aziz. is the number of components. Gas pseudocritical temperature (Tpc) are, respectively, sure (ppc) expressed as and where pciand T,; are critical pressure and critical temperature of components. deriving the A and B values from the flow-after-flow test. During reservoir depletion the thermodynamic equilibrium between kerogenlclays and the gas phase in the pore spaces changes. 3.4 Construction of Injlow Performance Relationship Cuwe 47 & OLFNWR9LHZ&DOFXODWLRQ([DPSOH Table 3-7 Input Data and Solution Given by Empirical IPR.xlsa Instructions: 1) Update data; 2) Run Macro Solution and view results. 11. Within the United States, the largest portion of the gas resource is found in the Green River Basin of Utah (Ikoku 1984). A field is an area that consists of one or more reservoirs all related to the same structural feature. Therefore the gas gravity is where the apparent molecular weight of gas can be calculated on the basis of gas composition. I). Trial-and-Error Calculation: First trial: gh = 1,148,450 cfh Pipeline Design 233 234 Chapter 11 Transportation Third trial: gh = 1,148,450 cfh Pipeline Design 233 234 Chapter 11 Transportation Third trial: gh = 1,148,450 cfh Pipeline Design 233 234 Chapter 11 Transportation Third trial: gh = 1,148,450 cfh Pipeline Design 233 234 Chapter 11 Transportation Third trial: gh = 1,148,450 cfh Pipeline Design 233 234 Chapter 11 Transportation Third trial: gh = 1,148,450 cfh Pipeline Design 233 234 Chapter 11 Transportation Third trial: gh = 1,148,450 cfh Pipeline Design 233 234 Chapter 11 Transportation Third trial: gh = 1,148,450 cfh Pipeline Design 233 234 Chapter 11 Transportation Third trial: gh = 1,148,450 cfh Pipeline Design 233 234 Chapter 11 Transportation Third trial: gh = 1,148,450 cfh Pipeline Design 233 234 Chapter 11 Transportation Third trial: gh = 1,148,450 cfh Pipeline Design 233 234 Chapter 11 Transportation Third trial: gh = 1,148,450 cfh Pipeline Design 233 234 Chapter 11 Transportation Third trial: gh = 1,148,450 cfh Pipeline Design 233 234 Chapter 11 Transportation Third trial: gh = 1,148,450 cfh Pipeline Design 233 234 Chapter 11 Transportation Third trial: gh = 1,148,450 cfh Pipeline Design 233 234 Chapter 11 Transportation Third trial: gh = 1,148,450 cfh Pipeline Design 233 234 Chapter 11 Transportation Third trial: gh = 1,148,450 cfh Pipeline Design 233 234 Chapter 11 Transportation Third trial: gh = 1,148,450 cfh Pipeline Design 233 234 Chapter 11 Transportation Third trial: gh = 1,148,450 cfh Pipeline Design 233 234 Chapter 11 Transportation Third trial: gh = 1,148,450 cfh Pipeline Design 233 234 Chapter 11 Transportation Third trial: gh = 1,148,450 cfh Pipeline Design 233 234 Chapter 11 Transportation Third trial: gh = 1,148,450 cfh Pipeline Design 233 234 Chapter 11 Transportation Third trial: gh = 1,close to the assumed 1,186,759 cfh B. The solution given by the spreadsheet is shown in Table 11-1. This is not normally economic except in deepwater where the presence of concrete may interfere with preferred installation method. There has been a huge disparity between "proven" reserves and potential reserves. Results are shown in Table 2-1. Although the estimated size of the resource base seems 1.6 Future of the Natural Gas Industry 7 significant, the recovery of this type of gas may be limited owing to practical constraints. Because the substance of this book is virtually boundless, knowing what to omit was the greatest difficulty with its editing. 11.2.2.2.4 Check for Hydrotest Condition The minimum hydrotest pressure for gas lines is given in Table 1 1 4, and is equal to 1.25 times the design pressure for pipelines. F. D. The process is repeated for a total of 3 to 4 rates. They described the fractal-like sequence of gas production at different length scales. For the convenience of engineering applications, pseudopressures of sweet natural gases at various pressures and temperatures have been generated with PseudoP.xls. The authors believe that it requires many books to describe the foundation of knowledge in natural gas engineering. (2007) pointed out that Joshi's equation is optimistic for high-productivity reservoirs due to neglecting the effect of frictional pressure in the horizontal wellbore. It will eventually evolve into a serious energy crunch. Assume that the overall efficiency is 30% (1 hp = 2,544 Btuth). It takes the following form: where q = volumetric flow rate, Mcfd pp, = pseudocritical pressure, psia D = pipe internal diameter, in L = pipe length, ft p, = pseudocritical pressure T = average flowing temperature, OR Y, = gas gravity, air = 1.0 q, = gas deviation factor at Tb and pb, normally accepted as 1.0 Based on Equation (2.5) for pseudocritical pressure (Wichert and Aziz I Pr 1972), the values of the integral function h d p, have been calculated 0 for various gas-specific gravity values. The propagation criteria is more conservative and should be used where optimization of the wall thickness is not required or for pipeline installation methods. As a rule of thumb or unless qualified thereafter, it is recommended to use propagation criteria for pipeline diameters under 16 inches and collapse criteria for pipeline diameters above or equal to 16 inches. 97 6.1 Introduction 6.2 Nodal Analysis 97 6.2.1 Analysis with the Bottom Hole Node 98 6.2.2 Analysis with Wellhead Node 101 6.3 Production Forecast 7 Separation 97 106. .113 7.1 Introduction 113 7.2 Separation of Gas and Liquids 113 Contents 7 2.1 7 2.2 7 2.3 7 2.4 Principles of Separation 114 Types of Separators 115 Factors Affecting Separation 118 Separator Design 120 7.3 Stage Separation 129 7.4 Flash Calculation 131 7.5 Low-Temperature Separation 8 Dehydration 138 ...143 8.1 Introduction 8.2 Dehydration of Natural Gas 143 8 2.1 Water Content of Natura Gas Streams 8 2.2 Dehydration Systems 146 8 2.3 Glycol Dehydrator Design 155 8.3 vii 143 144 Removal of Acid Gases 167 8 3.1 Iron-Sponge Sweetening 168 8 3.2 Alkanolamine Sweetening 168 8 3.3 GlycolIAmine Process 169 8 3.4 Sulfinol Process 170 9 Compression and Cooling .173 9.1 Introduction 173 9.2 Types of Compressors 9.3 Selection of Reciprocating Compressors 9.3.1 Volumetric Efficiency 178 9 3.2 Stage Compressors 9.5 Selection of Rotary Blowers 10 Volumetric Measurement 10.1 Introduction 174 176 189 194199 199 10.2 Measurement with Orifice Meters 199 10.2 1 Orifice Equation 201 10.2.2 Recording Charts 206 10.2 3 Computation of Volumes 209 ... Table 1-1 shows composition of a typical natural gas. Stiel. 2.10 Real Gas Normalized Pressure Real gas normalized pressure n(p) is defined as where p, is the pseudoreduced pressure. The energy disruptions should be a genuine concern. For simplicity, illustrative examples will be based on the Weymouth equation. It is not the authors' intention to simply duplicate general information that can be found in other books. It indicates that methane is a major component of the gas mixture. Let yi be the mole fraction of component i, the apparent molecular weight of the gas can be formulated using mixing rule as where M W; is the molecular weight of component i, and N. King (2010) summarized the evolution of the fracturing technique for shale gas formations. Equation (3.1) can be approximated using pressure approach as: where Bg is the average formation volume factor of gas in rblscf. The values of the constants are given in Table 1 1 4 for the different pipeline flow equations. It should be very difficult, if not impossible, to couple the Darcy gas flow in the nanopores, not mentioning that there are several levels of fractal-like scales (Javadpour et al., 2007) in addition to the hydraulic fractures which is the largest scale of flow network in shale gas reservoirs. 4 Wellbore radial flow in the fracture to the wellbore, where a "choking" effect occurs. Table 11-2 presents typical values of efficiency factors. For export lines, when P, is applied on a platform deck, the head of fluid shall be added to Pi for the pipelme section on the seabed (particularly for two-phase flow). The usage factor (11) is defined in Table 11-6 for gas lines. If the gas composition is not known but gas-specific gravity is given, the pseudocritical pressure and temperature can be determined from various charts or correlations developed based on the charts. Because natural gas is a complex mixture of light hydrocarbons with a minor amount of inorganic compounds, it is always desirable to find the composition of the gas through measurements. Oligney, A. The reservoir fracture dorizontal W ellbore Pwf Figure 3-4 Fluid low in a fracture to a horizontal Wells 53 where zei is half the distance between the ith and (i+1)Ih fractures, zsi is the permeability of the altered zone near the surface of fracture i, and pr represents the pressure in the fracture before the onset of flow convergence to wellbore (Figure 3-4). The United States has the world's largest economy and is by far the most voracious user of energy. This equation is also coded in the spreadsheet program Hall-Yarborogh-z.xls. DnV 1981 defines Pias the Maximum Allowable Operating Pressure (MAOP) under normal conditions, indicating that surge pressure up to 110% MAOP is acceptable. Dynamic viscosity (pg) in centipoises (cp) is usually used in the natural engineering: Kinematic viscosity (vg) is related to the dynamic viscosity (pg) is used, the well deliverability through n uniformly distributed fractures can be expressed as: 5. upper conservaedge of the loading conditions is required (T, and E ~)An tive limit is necessary and must often be estimated. In this chapter we recommend the following procedure for designing pipeline wall thickness: 11.2 Pipeline Design 25.1.1 Calculate the minimum wall thickness required for the design-internal pressure. Table 11-2 Typical Values of Efficiency 6, the transmission Factor In addition to the pipeline efficiency 6, the transmission factor 6 in Equation (1 1.22) is used for further tuning the theoretical pipeline flow equations. Of these, eastern Kentucky and western West Virginia are considered the most important. J., R. Geology. gives q = 1,645 Mscfld 3) Use backpressure model with real gas pseudopressure: gives q = 1,656 Mscfld 3.4 Construction of Inflow Performance Relationship Curve 43 & OLFNWR9LHZ&DOFXODWLRQ([DPSOH Table 3 4 Results Given by Empirical Deliverability.x]s (Continued) 4) Use backpressure model with pressure-squared approach: gives q = 1,648 Mscfld 3.4 Construction of Inflow Performance Relationship Curve 43 & OLFNWR9LHZ&DOFXODWLRQ([DPSOH Table 3 4 Results Given by Empirical Deliverability.x]s (Continued) 4) Use backpressure model with pressure-squared approach: gives q = 1,648 Mscfld 3.4 Construction of Inflow Performance Relationship Curve 43 & OLFNWR9LHZ&DOFXODWLRQ([DPSOH Table 3 4 Results Given by Empirical Deliverability.x]s (Continued) 4) Use backpressure model with pressure-squared approach: gives q = 1,648 Mscfld 3.4 Construction of Inflow Performance Relationship Curve 43 & OLFNWR9LHZ&DOFXODWLRQ([DPSOH Table 3 4 Results Given by Empirical Deliverability.x]s (Continued) 4) Use backpressure model with pressure-squared approach: gives q = 1,648 Mscfld 3.4 Construction of Inflow Performance Relationship Curve 43 & OLFNWR9LHZ&DOFXODWLRQ([DPSOH Table 3 4 Results Given by Empirical Deliverability.x]s (Continued) 4) Use backpressure model with pressure-squared approach: gives q = 1,648 Mscfld 3.4 Construction of Inflow Performance Relationship Curve 43 & OLFNWR9LHZ&DOFXODWLRQ([DPSOH Table 3 4 Results Given by Empirical Deliverability.x]s (Continued) 4) Use backpressure model with pressure-squared approach (Given by Empirical Deliverability.x]s (Continued) 4) Use backpressure model with pressure-squared approach (Given by Empirical Deliverability.x]s (Continued) 4) Use backpressure model with pressure-squared approach (Given by Empirical Deliverability.x]s (Continued) 4) Use backpressure model with pressure-squared approach (Given by Empirical Deliverability.x]s (Continued) 4) Use backpressure model with pressure-squared approach (Given by Empirical Deliverability.x]s (Continued) 4) Use backpressure model with pressure model wit an empirical equation, it can be used to construct well IPR curves. Solution This problem is solved with the spreadsheet program Brill-Beggs-Z.xls. Perhaps the best way to evaluate shale gas well productivity is to use the mathematical model presented in section 3.6 with validation by data from well deliverability testing. When pressure p is entered in psia, volume V in ft3, and temperature in OR, the gas constant R is equal to mole - " R 22 Chapter 2 Properties of Natural Gas The gas compressibility factor can be determined on the basis of measurements in PVT laboratories. Codes do not require that the pipeline be designed for hydrotest conditions, but sometimes give a tensile hoop stress limit 90% the specified minimum yield strength (SMYS) which is always satisfied if credit has not been taken for external pressure. Raghavan and Joshi (1993) presented a mathematical model that can predict the productivities of horizontal wells with multiple transverse fractures. In some cases, Piis defined as Wellhead Shut-In Pressure (WSIP) or specified by the operators. Dr. Boyun Guo ChevronTexaco Endowed Professor in Petroleum Engineering University of Louisiana at Lafayette Dr. Ali Ghalambor American Petroleum Institute Endowed Professor University of Louisiana at Lafayette Dr. Ali Ghalambor American Petroleum Engineering University of Louisiana at Lafayette Dr. Ali Ghalambor American Petroleum Engineering University of Louisiana at Lafayette Dr. Ali Ghalambor American Petroleum Institute Endowed Professor University of Louisiana at Lafayette Dr. Ali Ghalambor American Petroleum Engineering University of Louisiana at Lafayette Dr. Ali Ghalambor American Petroleum Engineering University of Louisiana at Lafayette Dr. Ali Ghalambor American Petroleum Engineering University of Louisiana at Lafayette Dr. Ali Ghalambor American Petroleum Engineering University of Louisiana at Lafayette Dr. Ali Ghalambor American Petroleum Engineering University of Louisiana at Lafayette Dr. Ali Ghalambor American Petroleum Engineering University of Louisiana at Lafayette Dr. Ali Ghalambor American Petroleum Engineering University of Louisiana at Lafayette Dr. Ali Ghalambor American Petroleum Engineering University of Louisiana at Lafayette Dr. Ali Ghalambor American Petroleum Engineering University of Louisiana at Lafayette Dr. Ali Ghalambor American Petroleum Engineering University of Louisiana at Lafayette Dr. Ali Ghalambor American Petroleum Engineering University of Louisiana at Lafayette Dr. Ali Ghalambor American Petroleum Engineering University of Louisiana at Lafayette Dr. Ali Ghalambor American Petroleum Engineering University of Louisiana at Lafayette Dr. Ali Ghalambor American Petroleum Engineering University of Louisiana at Lafayette Dr. Ali Ghalambor American Petroleum Engineering University of Louisiana at Lafayette Dr. Ali Ghalambor American Petroleum Engineering University of Louisiana at Lafayette Dr. Ali Ghalambor American Petroleum Engineering University of Louisiana at Lafayette Dr. Ali Ghalambor American Petroleum Engineering University of Louisiana Nomenclature xvii 1 Introduction ..1 1.1 What Is Natural Gas? Depending upon gas composition, espec~allythe content of inorganic compounds, the heating value of natural gas usually varies from 700 Btulscf. Proved reserves are those quantities of gas that have been found by the drill. It provided close to 24 percent of U.S. energy sources over the three-year period of 2000 to 2002. "International Energy Outlook." Energy Information Administration, Department of Energy, Washington DC, 2001. In order to avoid the impending energy crunch, more producers are switching from oil to natural gas. In crude the early years of the natural gas industry, when gas acco~np;~nied oil, it had to find a market or be flared; in the absence of eftective conservation practices, oil-well gas was often flared in huge quantities. Gas expansion factor is defined, in scf/ft3, as: in scf/rb. Natural Gas Production Engineering. It can be rewritten as: 254 Chapter I I Transportation For the reel barge method, the preferred pipeline grade is below X-60. If two test points are (ql,p w f l) and (q2,pwfl), expressions of these constants. Yarborough. Therefore, the gas flow can be considered isothermal at an average effective temperature without causing significant error in longpipeline calculations. The high variability was believed to be due to the local changes in permeability as a result of fracture intensity and fracture aperture width (U'eida et al., 2005). This book also gathers the authors' experiences gained through years of teaching the course of natural gas engineering at ulivc.rsities. It indicates that the demand of the world's economy for energy is ever increasing. &OLFNWR9LHZ&DOFXODWLRQ([DPSOH Table 11-5 Input Data and 6 in Segment length: 10 mi 4 and 6 in Segment length: 7 and 3 mi Parallel pipe ID: 4, 6, and 4 in Segment lengths: 3and 7 Series pipe ID: Solution Capacity improvement by series pipelines: Capacity improvement by parallel pipelines: Capacity improvement by receive a contains many different empirical transmission factors that have been used to meet the needs of pipelines: Capacity improvement by parallel pipelines: Capacity improvement by contains many different empirical transmission factors that have been used to meet the needs of pipelines: Capacity improvement by contains many different empirical transmission factors that have been used to meet the needs of pipelines: Capacity improvement by contains many different empirical transmission factors that have been used to meet the needs of pipelines: Capacity improvement by contains many different empirical transmission factors that have been used to meet the needs of pipelines: Capacity improvement by contains many different empirical transmission factors that have been used to meet the needs of pipelines: Capacity improvement by contains many different empirical transmission factors that have been used to meet the needs of pipelines: Capacity improvement by contains many different empirical transmission factors that have been used to meet the needs of pipelines: Capacity improvement by contains many different empirical transmission factors that have been used to meet the needs of pipelines: Capacity improvement by contains many different empirical transmission factors that have been used to meet the needs of pipelines: Capacity improvement by contains many different empirical transmission factors that have been used to meet the needs of pipelines: Capacity improvement by contains many different empirical transmission factors that have been used to meet the needs of pipelines: Capacity improvement by contains many different empirical transmission factors that have been used to meet the needs of pipelines transmission factors transmis of gas transportation in pipelines. The processes by which the parent organic material is converted into petroleum are not understood. Determination of the pseudopressure at a given pressure of Natural Gas laboratory and reported in mole fractions of components in the gas. Appendix A presents real gas pseudopressure charts for sweet natural gase\. 2-2 Calculate gas compressibility factors of a 0.65 specific gravity gas at 150 OF and 50 psia, and 5,000 psia, and 5,000 psia with Hall- 2.12 Problems Yarborough method. 7 Credit can be taken for external pressure for gathering lines or flowlines when the MAOP (Pi) is applied at the wellhead or at the seabed. 2.12 Problems 2-1 Estimate gas viscosities of a 0.70 specific gravity gas at 200 OF and 100 psia, 1,000 psia, and 10,000 psia.

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