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can be selected for low-pressure, large diameter pipelines to reduce material cost, or can be selected to require high ductility for improved impact resistance, which are valid for H2S < 3%, N2 < 5%, and total content of inorganic compounds less than 7%. Credit can be taken for oil export lines to account for head of fluid and for lines that traverse from deep to shallow water. Example Problem 3.3 Construct IPR curve for the well specified in Example Problem 3.1 with both pressure and pressure-squared approaches. The assumption is justified for work with commercial transmission lines. Corrosion allowance is made to account for damage during fabrication, transportation, and storage. Quantities of gas can be stored either as a dissolved phase in liquid hydrocarbons, or as an adsorbed phase on other materials within the shales of the kerogen, i.e., certain forms of illite. When one standard cubic feet of natural gas is combusted, it generates 700 Btu to 1,600 Btu 1.2 Utilization of Natural Gas 3 of heat, depending upon gas composition. 1 15000 loo00 u 34 5000 3 0 1920 1930 1940 1950 1960 1970 1980 1990 2000 2010 Figure 1-3 U.S. natural gas production history (Louisiana Department of Natural Resources 2011). Following the sequence of natural gas production, this book presents its contents in twelve chapters. 2.9 Real Gas Pseudopressure 29 &OLFNWR9LHZ&DOFXODWLRQ(DPSOH Table 2-5 Input Data and Calculated Parameters Given by PseudoP.xlsa Input Data .- Base pressure: 14.7 psia Maximum pressure: 10,000 psia Temperature: - Gas-specific gravity: 0.6 1 for air Mole fraction of N2: 0 Mole fraction of CO2: 0 Mole fraction of H2S: 0 Calculated Parameter Values Pseudocritical pressure: 673 psia .- Pseudocritical temperature: 357.57 OR .- Uncorrected gas viscosity at 14.7 psia: 0.010504 cp - N2 correction for gas viscosity at 14.7 psia: a. The pseudopressure is widely used for mathematical modeling of IPR of gas wells. Radial flow may prevail later if the drainage area is sufficiently large compared to the fractured region of the reservoir. Figure 3-4 illustrates flow in the fracture. 11.2.1.6 Practical Pipeline Equations 11.2.1.6.1 Pipeline Efficiency All pipeline flow equations were developed for perfectly clean lines filled with gas. This book fills the gap. Solution Output power of the generator: 1,000 kW = (1,000 kW)(3,412 Btu/h per kW) 4 Chapter 1 Introduction Fuel gas requirement: (8.19 x 10⁷ Btu/day)/(1,598 Btu/scf)/(0.5) = 1.025 x 10⁵ scf/day = 102.5 Mscf/day 1.3 Natural Gas Industry Natural gas was once a by-product of crude oil production. Apart from its obvious applications as a storable and transportable form of natural gas, LNG has many applications in its own right, particularly as a nonpolluting fuel for aircraft and ground vehicles. A rich or heavy gas reservoir may have a gravity equal to 0.75 or, in some rare cases, higher than 0.9. 2.3 Pseudocritical Properties Similar to gas apparent molecular weight, the critical properties of a gas can be determined on the basis of the critical properties of compounds in the gas using the mixing rule. Assume that the overall efficiency is 50 percent (1 kW = 3,412 Btu/h). There are often scales and even "j" u n k left in the line. The nominal pipeline wall thickness (tNOM) can be calculated as follows: where Pd is the design internal pressure defined as the difference between the internal pressure (Pi) and external pressure (Pe); D is nominal outside diameter; t is thickness allowance for corrosion; and, ayis the specified minimum yield strength. Gas wells are wells with producing gas-oil-ratio (GOR) being greater than 100,000 scf/stb; 2 Chapter 1 Introduction Table 1-1 I Composition of a Typical Natural Gas Compound I Methane Mole Fraction 0.8407 I Ethane 0.0586 I propane I 0.0220 I Hexane 0.0028 I / 1 -1 and Heavier 1 Carbon Dioxide 1 Hydrogen Sulfide I 1.0063 I Nitrogen 0.0345 Total 1.0000 - \$ condensate wells are those with producing GOR being less than 100,000 scf/stb but greater than 5,000 scf/stb; and wells with producing GOR being less than 5,000 scf/stb are classified as oil wells. For a uniform slope, Le is defined as For a nonuniform slope (where elevation change cannot be simplified to a single section of constant gradient), an approach in steps to any number of sections, n, will yield where 11.2.15. Both the back pressure model and the Forchheimer model can be used to analyze the test data. 2020 9 10 Chapter 1 Introduction 1.7 References Allison, I. If gas composition and viscosities of gas components are known, the mixing rule can be used for determining the viscosity of the gas mixture: Gas viscosity is very often estimated with charts or correlations developed based on the charts. Taking air molecular weight 29 and R = 10.73 psia - ft³ mole⁻¹ ° R, Equation (2.43) is rearranged to yield: where the gas density is in lbm/ft³. Combining Equations (3.19) through (3.22) yields a reservoir deliverability equation, expressed as: where 54 Chapter 3 Gas Reservoir Deliverability 3.7 Shale Gas Wells Shale gas is natural gas produced from shale sequences. The twentieth century was the century of oil that was the primary energy source to support the growth of global economy. 232 Chapter 11 Transportation Example Problem 1.1 For the following data given for a horizontal pipeline, predict gas flow rate in cubic ft/hr through the pipeline. Associated or dissolved gas is found with crude oil. "Natural Gas: Beyond All Expectations." Paper SPE 7 15 12 presented at the 2001 SPE Annual Technical Conference and Exhibition, New Orleans, Louisiana, September 30-October 3, 2001. Society of Petroleum Engineers of AIME, Dallas, 1977. Applying the Weymouth equation to the third segment (with diameter D3) yields: Adding equations (1.1.56) and (1.1.57) results in: 246 Chapter 1 I Transportation Capacity of a single-diameter (D3) pipeline is expressed as: Dividing Equation (1.1.59) by Equation (1.1.60) yields: Let Y be the fraction of looped pipeline and X be the increase in gas capacity. Equation (1.1.61) can be rearranged as: where RD is ratio of the looping pipe diameter to the original pipe diameter. Direct measurements of gas viscosity are preferred for a new gas. Compression and Cooling 10. If possible, the final flow period should be long enough to achieve stabilized flow condition. (2007) presented experimentally obtained permeabilities of 152 samples from nine shale gas reservoirs with pore- 3.7 Shale Gas Wells 55 size distribution of several shale samples at 60,000 psi mercury injection pressure. Some estimates were based on growth curves, extrapolations of past production, exploratory footage drilled, and discovery rates. 3.8 Well Deliverability Testing Well deliverability testing provides a direct means of estimating productivity of gas wells. A pool contains one or more resin oils in isolated structures. The efficiency factor expresses the actual flow capacity as a fraction of the theoretical flow rate. Natural gas accumulations in geological traps can be classified as reservoir, field, or pool. Input Data Reservoir pressure: 4,505 psia Test point 1, flow rate: 1,152 Mscf/d bottom hole pressure 3,025 psia Test point 2, flow rate: 1,548 Mscf/d bottom hole pressure 1,685 psia Solution log(S) n = 2 p2 - Pwf 1 1 0 g IP2 a. 11.2 Pipeline Design 23 1 The heat of compression is usually dissipated into the ground along a pipeline within a few miles downstream from the compressor station. The result is shown in Table 2-2. This must-have handbook includes: A focus on real-world needs rather than theory; Illustrative examples throughout the text; Spreadsheet programs for all the engineering calculations; Exercise problems at the end of every chapter, including newly added questions utilizing the spreadsheet programs; Newly expanded sections covering today's technologies, such as multi-fractured horizontal wells and shale gas wells; Content: Front Matter • List of Spreadsheet Programs • Spreadsheet Programs and Functions • List of Nomenclature • Preface • Table of Contents I. Palmer. 3.8 0 10 20 30 Well Deliverability Testing 40 50 60 70 57 80 T 1 m e (months) Figure 3-5 Gas production curves of 3 wells in a 1-sq. Natural gas is the only fuel that is superior to other energy sources in economic attractiveness and environmental concerns. The philosophy involved in deriving the special relationships used in the solution of complex transmission systems is to express the various lengths and diameters of the pipe in the systems as equivalent lengths of common diameter or equivalent diameter of a common length, there equivalent means that both lines will have the same capacity with the same total pressure drop. At the receiving terminals, the LNG is reconverted to a gaseous state by passage through a regasifying plant, whence it can be fed as required into the normal gas distribution grid of the importing country. (2005) published a comprehensive description of pipeline design, installation, and operations for offshore and deepwater development. B. Input Data Effective permeability to gas: 0.17 md Pay zone thickness: 78 ft Equivalent drainage radius: Wellbore radius: 0.328 ft Darcy skin factor: 5 Non-Darcy coefficient: 0.001 d/Mscf Reservoir pressure: 4,613 psia Temperature: 180 ° F The average gas viscosity: 0.022 cp The average gas compressibility factor: Effective permeability to gas: a. MW y i ~ ~ Pci MW, = 20.71 y i = 0.71 (psia) YiPci (psia) (OR) yiTci ("R) ppc = 661 Tpc = 41 1 Tci This spreadsheet calculates gas apparent molecular weight, specific gravity, pseudocritical pressure, and pseudocritical temperature. Spiral well pipe is very unusual for gas pipelines and should be used only for low-pressure water or outfall lines. Properties of Natural Gas 3. Aziz. is the number of components. Gas pseudocritical presand pseudocritical temperature (Tpc) are, respectively, sure (ppc) expressed as and where pciand Tc; are critical pressure and critical temperature of component i, respectively. Figure 3-8 shows the data plot and technique for deriving the A and B values from the flow-after-flow test. During reservoir depletion the thermodynamic equilibrium between kerogenclays and the gas phase in the pore spaces changes. 3.4 Construction of Inflow Performance Relationship Curve 47 &OLFNWR9LHZ&DOFXODWLRQ(DPSOH Table 3-7 Input Data and Solution Given by Empirical IPR.xlsa Instructions: 1) Update data; 2) Run Macro Solution and view results. 11. Within the United States, the largest portion of the gas resource is found in the Green River Basin of Wyoming, the Piceance Basin of Colorado, and the Uinta Basin of Utah (Ikoku 1984). A field is an area that consists of one or more reservoirs all related to the same structural feature. Therefore the gas gravity is where the apparent molecular weight of gas can be calculated on the basis of gas composition. I). Trial-and-Error Calculation: First trial: qh = 1,148,450 cfm Second trial: qh = 1,148,450 cfm Pipeline Design 233 234 Chapter 11 Transportation Third trial: qh = 1,186,759 cfm qh = 1,187,962 cfm which is close to the assumed 1,186,759 cfm B. The solution given by the spreadsheet is shown in Table 11-1. This is not normally economic except in deepwater where the presence of concrete may interfere with preferred installation method. There has been a huge disparity between "proven" reserves and potential reserves. Results are shown in Table 2-1. Although the estimated size of the resource base seems 1.6 Future of the Natural Gas Industry 7 significant, the recovery of this type of gas may be limited owing to practical constraints. Because the substance of this book is virtually boundless, knowing what to omit was the greatest difficulty with its editing. 11.2.2.2.2.4 Check for Hydrotest Condition The minimum hydrotest pressure for gas lines is given in Table 1 1 4 , and is equal to 1.25 times the design pressure for pipelines. F. D. The process is repeated for a total of 3 to 4 rates. They described the fractal-like sequence of gas production at different length scales. For the convenience of engineering applications, pseudopressures of sweet natural gases at various pressures and temperatures have been generated with PseudoP.xls. The authors believe that it requires many books to describe the foundation of knowledge in natural gas engineering. (2007) pointed out that Joshi's equation is optimistic for high-productivity reservoirs due to neglecting the effect of frictional pressure in the horizontal wellbore. It will eventually evolve into a serious energy crunch. Assume that the overall efficiency is 30% (1 hp = 2,544 Btu/h). It takes the following form: where q = volumetric flow rate, Mcf/d pp = pseudocritical pressure, psia D = pipe internal diameter, in L = pipe length, ft p = pseudoreduced pressure T = average flowing temperature, OR Y, = gas gravity, air = 1.0 q = gas deviation factor at Tb and pb, normally accepted as 1.0 Based on Equation (2.5) for pseudocritical pressure (Wichert and Aziz Pr 1972), the values of the integral function h d p , have been calculated 0 for various gas-specific gravity values. The propagation criteria is more conservative and should be used where optimization of the wall thickness is not required or for pipeline installation methods not compatible with the use of buckle arrestors such as reel and tow methods. As a rule of thumb or unless qualified thereafter, it is recommended to use propagation criteria for pipeline diameters under 16 inches and collapse criteria for pipeline diameters above or equal to 16 inches. 97 6.1 Introduction 6.2 Nodal Analysis 97 6.2.1 Analysis with the Bottom Hole Node 98 6.2.2 Analysis with Wellhead Node 101 6.3 Production Forecast 7 Separation 97 106113 7.1 Introduction 113 7.2 Separation of Gas and Liquids 113 Contents 7 2 1 7 2 2 7 2 3 7 2.4 Principles of Separation 114 Types of Separators 115 Factors Affecting Separation 118 Separator Design 120 7.3 Stage Separation 129 7.4 Flash Calculation 131 7.5 Low-Temperature Separation 8 Dehydration 138143 8.1 Introduction 8.2 Dehydration of Natural Gas 143 8 2 1 Water Content of Natural Gas Streams 8 2 2 Dehydration Systems 146 8 2 3 Glycol Dehydrator Design 155 8 3 vii 143 144 Removal of Acid Gases 167 8 3 1 Iron-Sponge Sweetening 168 8 3 2 Alkanolamine Sweetening 168 8 3 3 GlycolAmine Process 169 8 3 4 Sulfinol Process 170 9 Compression and Cooling173 9 1 Introduction 173 9 2 Types of Compressors 9 3 Selection of Reciprocating Compressors 9 3 1 Volumetric Efficiency 178 9 3 2 Stage Compression 179 9 3 3 Isentropic Horsepower 181 9 4 Selection of Centrifugal Compressors 9 5 Selection of Rotary Blowers 10 Volumetric Measurement 10 1 Introduction 174 176 189 194199 199 10 2 Measurement with Orifice Meters 199 10 2 1 Orifice Equation 201 10 2 2 Recording Charts 206 10 2 3 Computation of Volumes 209 Table 1-1 shows composition of a typical natural gas. Stiel. 2.10 Real Gas Normalized Pressure Real gas normalized gas pressure n(p) is defined as where p, is the pseudoreduced pressure. The energy disruptions should be a genuine concern. For simplicity, illustrative examples will be based on the Weymouth equation. It is not the authors' intention to simply duplicate general information that can be found in other books. It indicates that methane is a major component of the gas mixture. Let yi be the mole fraction of component i, the apparent molecular weight of the gas can be formulated using mixing rule as where MW is the molecular weight of component i, and N, King (2010) summarized the evolution of the fracturing technique for shale gas formations. Equation (3.1) can be approximated using pressure approach as: where Bg is the average formation volume factor of gas in rblscf. The values of the constants are given in Table 1 1 4 for the different pipeline flow equations. It should be very difficult, if not impossible, to couple the Darcy gas flow in fractures with the nanoscale gas flow in the nanopores, not mentioning that there are several levels of fractal-like scales (Javadpour et al., 2007) in addition to the hydraulic fractures which is the largest scale of flow network in shale gas reservoirs. 4 Wellbore radial flow in the fracture to the wellbore, where a "choking" effect occurs. Table 11-2 presents typical values of efficiency factors. For export lines, when P is applied on a platform deck, the head of fluid shall be added to Pi for the pipeline section on the seabed (particularly for two-phase flow). The usage factor (11) is defined in Table 11-6 for gas lines. If the gas composition is not known but gas-specific gravity is given, the pseudocritical pressure and temperature can be determined from various charts or correlations developed based on the charts. Because natural gas is a complex mixture of light hydrocarbons with a minor amount of inorganic compounds, it is always desirable to find the composition of the gas through measurements. Oligney, A. The reservoir-fracture cross-flow model of Guo and Schechter (1997) gives: 52 Chapter 3 Gas Reservoir Deliverability Fracture Horizontal Wellbore Figure 3-3 A reservoir section drained by a multi-fractured horizontal wellbore Pwf Figure 3-4 Fluid flow in a fracture to a horizontal wellbore 3.6 Multi-Fractured Horizontal Wells 53 where z is half the distance between the ith and (i+1)th fractures, zsi is the depth of the altered zone near the surface of fracture i, ksi is the permeability of the altered zone near the surface of fracture i, and pi represents the pressure in the fracture before the onset of flow convergence to wellbore (Figure 3-4). The United States has the world's largest economy and is by far the most voracious user of energy. This equation is also coded in the spreadsheet program Hall-Yarborough-z.xls. DNV 1981 defines Pias the Maximum Allowable Operating Pressure (MAOP) under normal conditions, indicating that surge pressure up to 110% MAOP is acceptable. Dynamic viscosity (pg) in centipoises (cp) is usually used in the natural engineering; Kinematic viscosity (vg) is related to the dynamic viscosity through density (pg) 18 Chapter 2 Properties of Natural Gas Kinematic viscosity is not normally used in natural gas engineering. (2003) is used, the well deliverability through n uniformly distributed fractures can be expressed as: 5 . upper conservae dge of the loading conditions is required (T, and E ~ v) An tive limit is necessary and must often be estimated. In this chapter we recommend the following procedure for designing pipeline wall thickness: 11.2 Pipeline Design 25 1 1 Calculate the minimum wall thickness required for the design-internal pressure. Table 11-2 Typical Values of Efficiency Factors Type of Line I Casing-head gas I Gas and condensate I I Liquid Content (gall/Mscf) Efficiency E 0.1 0.92 7.2 800 I 0.77 0.6 1 240 Chapter 1 I Transportation 11.2.1.6.2 Transmission Factor In addition to the pipeline efficiency 6, the transmission factor 6 in Equation (1.1.22) is used for further tuning the theoretical pipeline flow equations. Of these, eastern Kentucky and western West Virginia are considered the most important. J., R. Geology, gives q = 1,645 Mscf/d 3) Use backpressure model with real gas pseudopressure: gives q = 1,656 Mscf/d 3.4 Construction of Inflow Performance Relationship Curve 43 &OLFNWR9LHZ&DOFXODWLRQ(DPSOH Table 3 4 Results Given by Empirical Deliverability.xls (Continued) 4) Use backpressure model with pressure-squared approach: gives q = 1,649 Mscf/d 3.4 Construction of Inflow Performance Relationship Curve Once a deliverability equation is established using either a theoretical or an empirical equation, it can be used to construct well IPR curves. Solution This problem is solved with the spreadsheet program Brill-Beggs-Z.xls. Perhaps the best way to evaluate shale gas well productivity is to use the mathematical model presented in section 3.6 with validation by data from well deliverability testing. When pressure p is entered in psia, volume V in ft³, and temperature in OR, the gas constant R is equal to mole⁻¹ ° R 22 Chapter 2 Properties of Natural Gas The gas compressibility factor can be determined on the basis of measurements in PVT laboratories. Codes do not require that the pipeline be designed for hydrotest conditions, but sometimes give a tensile hoop stress limit 90% the specified minimum yield strength (SMYS) which is always satisfied if credit has not been taken for external pressure. Raghavan and Joshi (1993) presented a mathematical model that can predict the productivities of horizontal wells with multiple transverse fractures. In some cases, Pias defined as Wellhead Shut-In Pressure (WSIP) or specified by the operators. Dr. Boyun Guo ChevronTexaco Endowed Professor in Petroleum Engineering University of Louisiana at Lafayette Dr. Ali Ghalambor American Petroleum Institute Endowed Professor University of Louisiana at Lafayette Contents Preface xi List of Spreadsheet Programs xv Spreadsheet Programs and Functions xvi List of Nomenclature xvii 1 Introduction 1 1.1 What Is Natural Gas? Depending upon gas composition, espec- allythe content of inorganic compounds, the heating value of natural gas usually varies from 700 Btu/scf to 1,600 Btu/scf. Proved reserves are those quantities of gas that have been found by the drill. It provided close to 24 percent of U.S. energy sources over the three-year period of 2000 to 2002. "International Energy Outlook." Energy Information Administration, Department of Energy, Washington DC, 2001. In order to avoid the impending energy crunch, more producers are switching from oil to natural gas. In crude the early years of the natural gas industry, when gas accompanied oil, it had to find a market or be flared; in the absence of effective conservation practices, oil-well gas was often flared in huge quantities. Gas expansion factor is defined, in scf/ft³, as: in scf/stb. Natural Gas Production Engineering. It can be rewritten as: 254 Chapter 1 I Transportation For the reel barge method, the preferred pipeline grade is below X-60. If two test points are (q1,p w f1) and (q2,pwf1), expressions of these constants are: A = [m(Fz - mPwf1) - B4]. It is obvious that a multirate test is required to estimate values of these constants. Yarborough. Therefore, the gas flow can be considered isothermal at an average effective temperature without causing significant error in longpipeline calculations. The high variability was believed to be due to the local changes in permeability as a result of fracture intensity and fracture aperture width (U'eida et al., 2005). This book also gathers the authors' experiences gained through years of teaching the course of natural gas engineering at uliv.ersities. It indicates that the demand of the world's economy for energy is ever increasing. &OLFNWR9LHZ&DOFXODWLRQ(DPSOH Table 11-5 Input Data and Solution Given by ~ooped~ines.xls(-) Input Data Original pipe ID: 4 in Total pipeline length: 10 mi 4 and 6 in Segment lengths: 7 and 3 mi Parallel pipe ID: 4and 6 in Looped pipe ID: 4, 6, and 4 in Segment lengths: 3and 7 Series pipe ID: Solution Capacity improvement by series pipelines: Capacity improvement by parallel pipelines: Capacity improvement by looped pipelines: a. Thus, the literature contains many different empiricaltransmission factors that have been used to meet the needs of pipeline engineers. Chapter 11 presents principles of gas transportation in pipelines. The processes by which the parent organic material is converted into petroleum are not understood. Determination of the pseudopressure at a given pressure requires knowledge of gas viscosity and z-factor as functions of pressure and temperature. Gas composition is usually determined in a 14 Chapter 2 Properties of Natural Gas laboratory and reported in mole fractions of components in the gas. Appendix A presents real gas pseudopressure charts for sweet natural gasel. 2-2 Calculate gas compressibility factors of a 0.65 specific gravity gas at 150 OF and 50 psia, 500 psia, and 5,000 psia with Hall- 2.12 Problems Yarborough method. 7 Credit can be taken for external pressure for gathering lines or flowlines when the MAOP (Pi) is applied at the wellhead or at the seabed. 2.12 Problems 2- 1 Estimate gas viscosities of a 0.70 specific gravity gas at 200 OF and 100 psia, 1,000 psia, 5,000 psia, and 10,000 psia.

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